

# Low dimensional model for control of the Blasius boundary layer by balanced truncation

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*in collaboration with*

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## Outline of talk

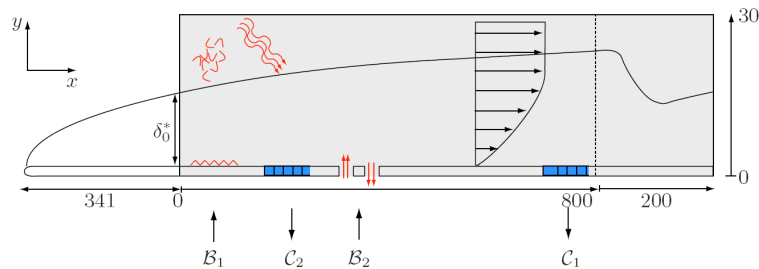
- Flow instability, examining the initial value problem
- Adding inputs and outputs: The lifting procedure for wall actuation
- Reduced order models preserving input-output characteristics, balanced truncation
- LQG feedback control results based on reduced order model
- Conclusions



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## Flow set up and state space form



- Linearized Navier-Stokes equations

$$\dot{\mathbf{u}} = \mathcal{A}\mathbf{u}$$

$$\mathbf{u} = \mathbf{u}_0 \quad \text{at} \quad t = 0.$$

- Evolution operator central to both stability investigation and control design

$$\mathbf{u}(t) = \mathcal{T}(t)\mathbf{u}_0 = \exp(\mathcal{A}t)\mathbf{u}_0$$

- Stability deals with full system



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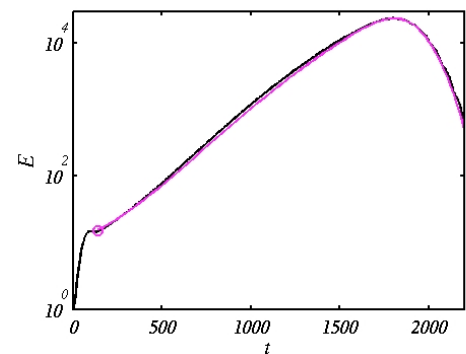
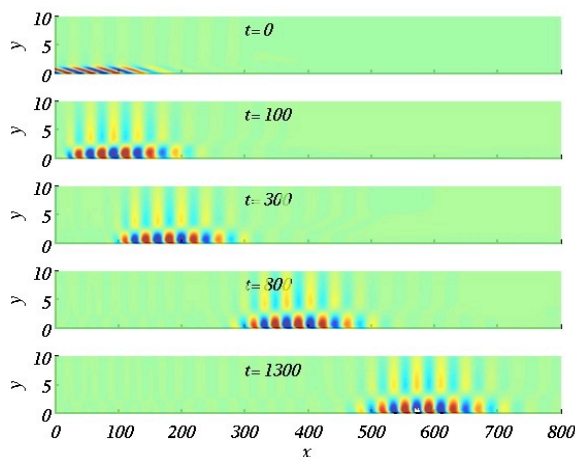
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## Non-modal growth

- Asymptotically stable; single eigenmodes are not observed
- Optimal growth computed from  $\sigma \hat{\mathbf{u}} = \mathcal{T}^\dagger(t_0)\mathcal{T}(t_0)\hat{\mathbf{u}}$  yields wavepacket propagation
- Orr/TS mechanism



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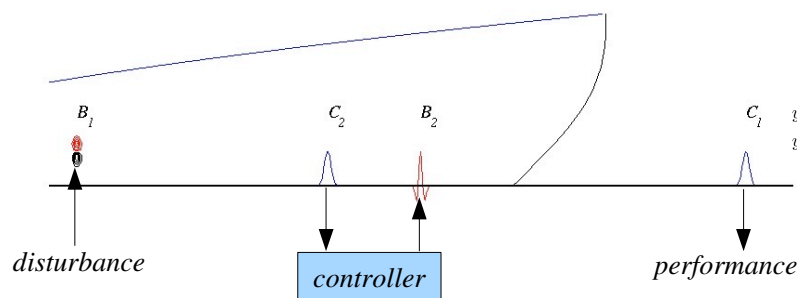
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## Adding inputs and outputs to the NS equations



$B_1\psi$  : External disturbances  
 $B_2\phi$  : Actuation  
 $y_1 = C_1\mathbf{u}$  : Sensor for feedback  
 $y_2 = C_2\mathbf{u}$  : Sensor for objective function

- Forced NS stokes equations with outputs

$$\dot{\mathbf{u}} = \mathcal{A}\mathbf{u} + B_1\psi + B_2\phi = \mathcal{A}\mathbf{u} + Bf \quad y = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} C_1\mathbf{u} \\ C_2\mathbf{u} \end{bmatrix} = C\mathbf{u}$$

- Input-output behaviour

$$y(t) = CT(t)\mathbf{u}_0 + C \int_0^t T(t-\tau)Bf(\tau)d\tau$$

- For control design it is sufficient to capture the I-O behaviour



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## Obtaining a state space formulation for wall actuation

- Boundary controlled system not on state space form

$$\dot{\mathbf{u}} = \mathcal{A}\mathbf{u}$$

$$\mathbf{u}(x, 0, t) = \mathbf{u}_w\varphi(t) = (0, v_w(x))^T\varphi(t),$$

- Lifting procedure to obtain a volume forced system (Högberg et al. 2003)

$$\mathbf{u} = \mathbf{u}_h + Z\varphi$$

- Steady state solution

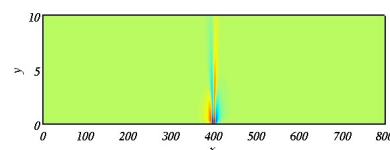
$$0 = \mathcal{A}Z$$

$$Z(x, 0) = \mathbf{u}_w = (0, v_w(x))^T$$

- Form an augmented system  $\hat{\mathbf{u}} = (\mathbf{u}_h, \varphi)^T$

$$\dot{\hat{\mathbf{u}}} = \hat{\mathcal{A}}\hat{\mathbf{u}} + \hat{B}_2\phi, \quad \text{with} \quad \hat{\mathcal{A}} = \begin{bmatrix} \mathcal{A} & 0 \\ 0 & 0 \end{bmatrix}, \quad \hat{B}_2 = \begin{bmatrix} -Z \\ 1 \end{bmatrix}, \quad \phi = \dot{\varphi}$$

steady state solution from DNS



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## Reduced order model for control

- Full system too big for optimization problem and online time integration

$$\begin{aligned}\dot{\mathbf{u}} &= \mathcal{A}\mathbf{u} + \mathcal{B}f \\ y &= \mathcal{C}\mathbf{u}\end{aligned}\quad n > 10^5$$

- Approximate by reduced system

$$\begin{aligned}\dot{\kappa} &= \hat{A}\kappa + \hat{B}f \\ \hat{y} &= \hat{C}\kappa\end{aligned}\quad m < 100$$

- Such that the IO is preserved

$$\|y - \hat{y}\| < \epsilon$$

- One systematic approach is balanced truncation (*Moore 81*)



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## Controllability and observability

- How do the inputs affect the outputs?
- Generated states from input (controllability)

$$\mathbf{u}_0 = \int_{-\infty}^0 \mathcal{T}(-\tau)\mathcal{B}f(\tau)dt = \mathcal{L}_c f$$

- Generated signal from states (observability)

$$y(t) = \mathcal{C}\mathcal{T}(t)\mathbf{u}_0 = \mathcal{L}_o(t)\mathbf{u}_0$$

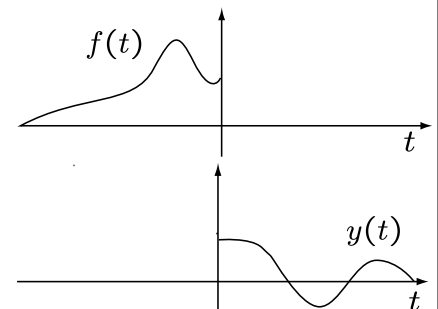
- Hankel operator

$$y(t) = \mathcal{L}_o(t)\mathcal{L}_c f(t) = (\mathcal{H}f)(t)$$

- Gramians

$$\mathcal{P} = \mathcal{L}_c \mathcal{L}_c^\dagger = \int_0^\infty \mathcal{T}(\tau)\mathcal{B}\mathcal{B}^\dagger\mathcal{T}^\dagger(\tau) d\tau$$

$$\mathcal{Q} = \mathcal{L}_o^\dagger \mathcal{L}_o = \int_0^\infty \mathcal{T}^\dagger(\tau)\mathcal{C}^\dagger\mathcal{C}\mathcal{T}(\tau) d\tau$$



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## Gramians

- Approximate integrals by quadrature (snapshots)

$$\mathcal{P} = \int_0^\infty T(\tau) \mathcal{B} \mathcal{B}^\dagger T^\dagger(\tau) d\tau \approx X X^T, \quad X = [\mathcal{B}, \exp(\mathcal{A}t_1)\mathcal{B}, \dots, \exp(\mathcal{A}t_n)\mathcal{B}]$$

$$\mathcal{Q} = \int_0^\infty T^\dagger(\tau) \mathcal{C}^\dagger \mathcal{C} T(\tau) d\tau \approx Y Y^T, \quad Y = [\exp(\mathcal{A}^\dagger t_m) \mathcal{C}^\dagger, \dots, \exp(\mathcal{A}^\dagger t_1) \mathcal{C}^\dagger, \mathcal{C}^\dagger]$$

- POD modes  $\text{eig}\{X X^T\}$ 
  - Ranks states most easily influenced by input
- Adjoint POD modes  $\text{eig}\{Y Y^T\}$ 
  - Ranks states most easily sensed by output

- Balanced modes mutually diagonalize Gramians

$$\mathcal{P} \mathcal{Q} \mathbf{v} = \sigma \mathbf{v} \quad \Rightarrow \quad \underbrace{X^T Y Y^T X}_{m \times m} \mathbf{a} = \sigma \mathbf{a}, \quad \mathbf{v} = X \mathbf{a}$$

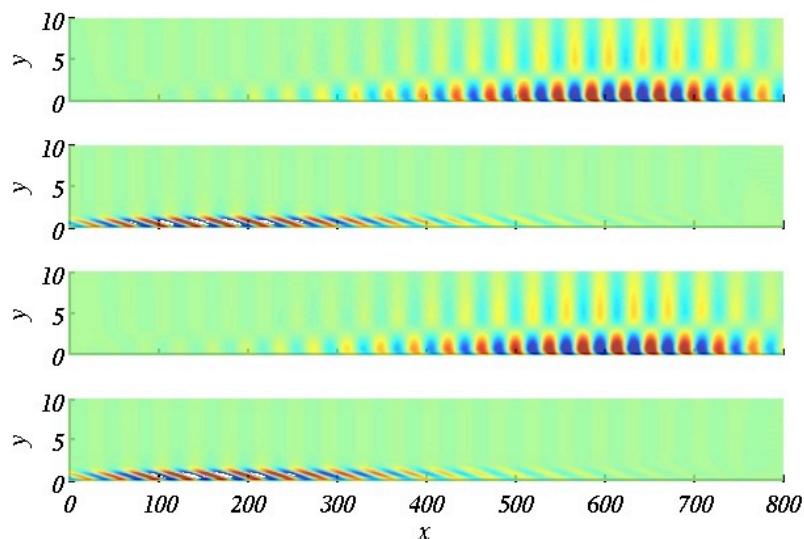


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## Balanced modes

- Direct and adjoint balanced modes



- Use these for oblique Galerkin projection to create reduced order model



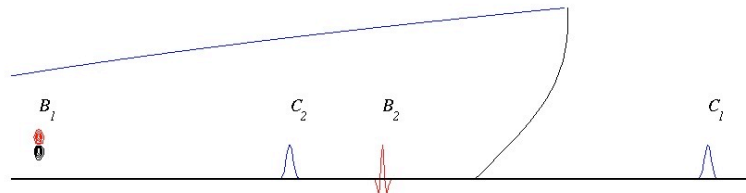
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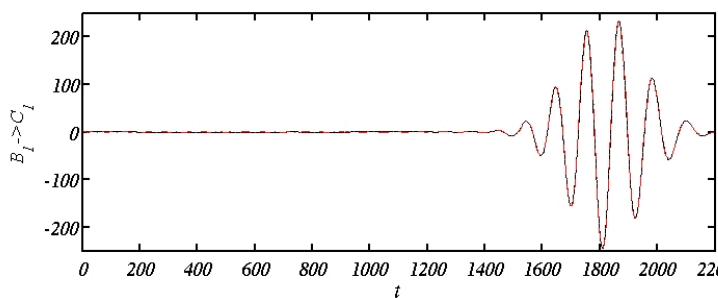
## Preserving input-output behaviour



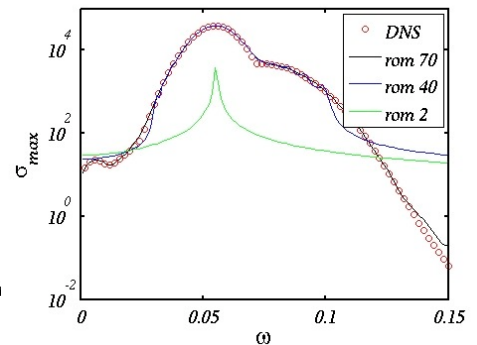
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Impulse response from disturbance to objective function



Frequency response from all inputs to all outputs



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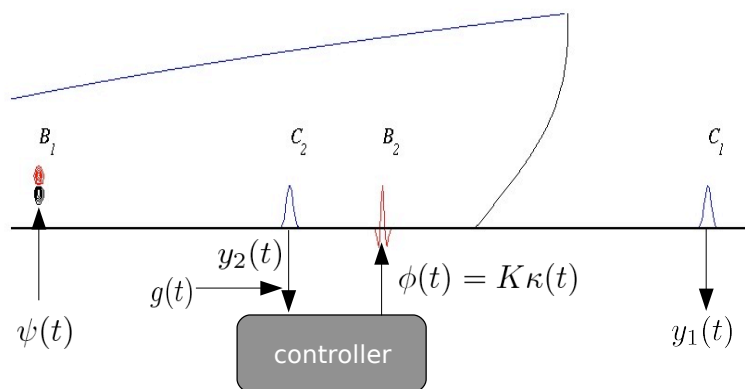
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## Optimal Feedback Control – LQG



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Find an optimal control signal  $\phi(t)$  based on the measurements  $y_2(t)$  such that in the presence of external disturbances  $\psi(t)$  and measurement noise  $g(t)$  the output  $y_1(t)$  is minimized.

→ Solution: LQG/H2

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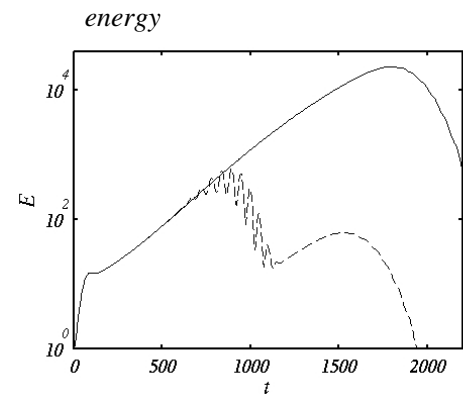
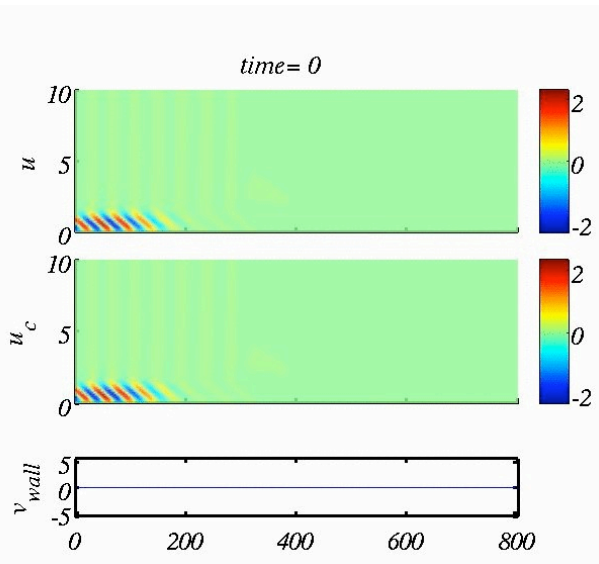
# Control of the propagating wavepacket

- Small estimator running online
- Control signal fed into actuator in DNS



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# Conclusions

- Balanced modes give low order models preserving input-output relationship between sensors and actuators
- Feedback control of Blasius flow
  - Impulse and frequency response well captures
  - Reduced order models with balanced modes used in LQG control
  - Controller based on small number of modes works well in DNS
- Framework enables LQG control for many complex flows
  - DNS/ADNS is all that is needed



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