

Vortex Particle Method for Simulation of Viscous Flows

Gdańsk, May 12-13, 2011

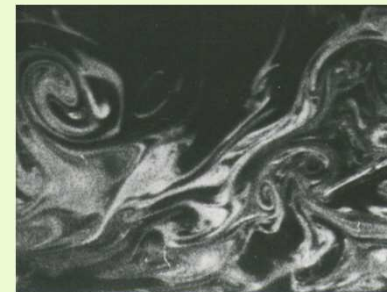
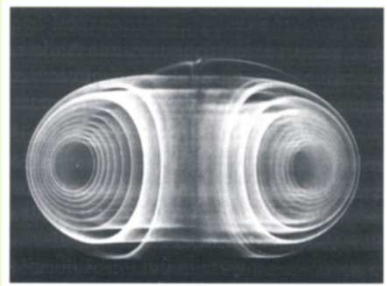
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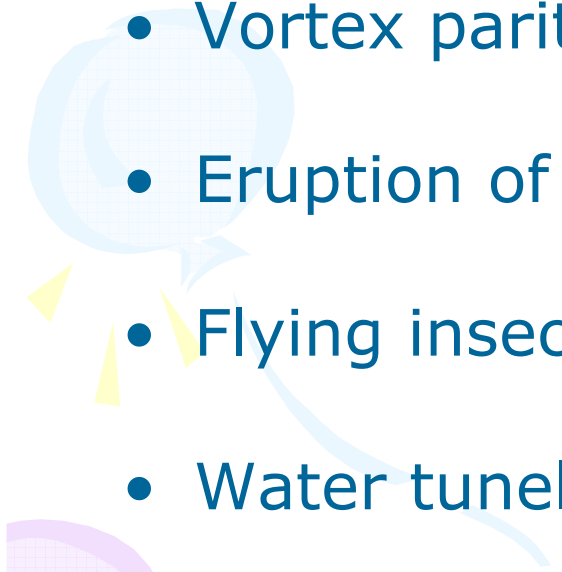

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POLAND





Outline of presentation:

- Fundamentals of Vortex Particle Methods - Kinematics of Vorticity,
 - Vortex particle method (VIC) in 2D
 - Eruption of Boundary Layer
 - Flying insects
 - Water tunnel
 - Vortex particle method (VIC) in 3D –Vortex Rings
 - Parallel computations
- 
- 



1. Equations of Motion

- Navier-Stokes equation:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \Delta \mathbf{u} \quad (1)$$

$$\nabla \cdot \mathbf{u} = 0$$

Equation (1) can be transformed to the vorticity transport equation:

$$\frac{\partial \boldsymbol{\omega}}{\partial t} + (\mathbf{u} \cdot \nabla) \boldsymbol{\omega} = (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} + \nu \Delta \boldsymbol{\omega}$$

where

$$\boldsymbol{\omega} = (\omega_1, \omega_2, \omega_3) = \nabla \times \mathbf{u} = \mathbf{rot}(\mathbf{u})$$



KINEMATICS OF VORTICITY

$$\nabla \cdot \mathbf{u} = 0$$

$$\mathbf{u} = \nabla \times \mathbf{A} \qquad \nabla \cdot (\nabla \times \mathbf{A}) \equiv 0$$

$$\nabla \times \mathbf{u} = \underline{\omega} \qquad \nabla \times (\nabla \times \mathbf{A}) = \nabla(\nabla \cdot \mathbf{A}) - \Delta \mathbf{A}$$

$\mathbf{A} = (A_1, A_2, A_3)$ - vector potential

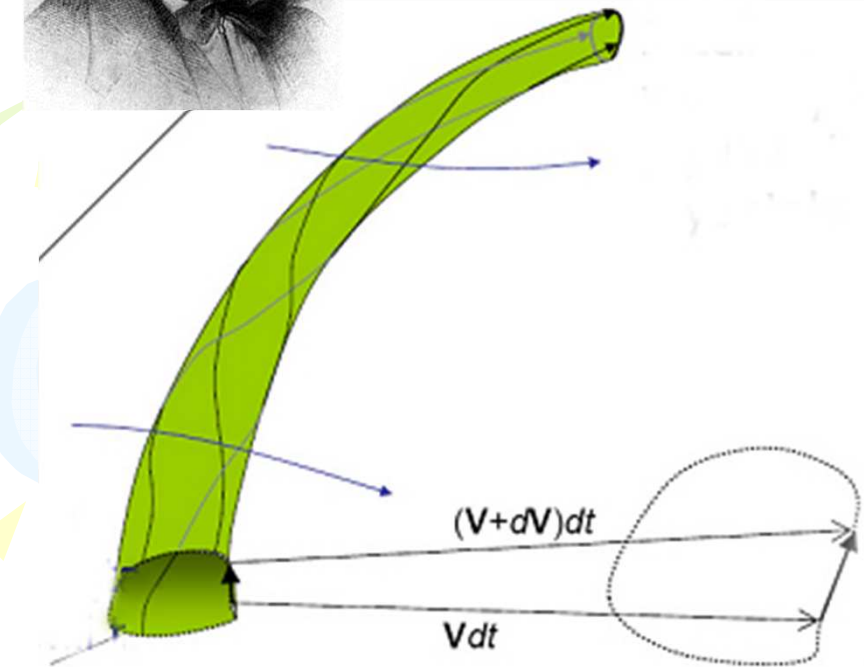
It is assumed that : $\nabla \cdot \mathbf{A} = 0$, więc

$$\Delta A_i = -\omega_i, \qquad i = 1, 2, 3$$



Helmholtz theorms

1. The strength of vortex tube is uniform along the tube
2. The strength (circulation about any closed circuit C) is invariant in time.
3. Vortex lines are material lines



Fluid loop at time t

The loop at time t+dt created by the same fluid particles

$$\frac{d \mathbf{x}}{dt} = \mathbf{v}(\mathbf{x})$$

(1) (3) \Leftrightarrow

$$\frac{d \underline{\omega}}{dt} = (\underline{\omega} \cdot \nabla) \mathbf{v}$$

Two -Dimensional simulation(2D)

$$\mathbf{A} = (0, 0, \psi) \quad \mathbf{u} = \nabla \times \mathbf{A} = (u, v, 0) = \left(\frac{\partial \psi}{\partial y}, -\frac{\partial \psi}{\partial x}, 0 \right)$$

$$\Delta \psi = -\omega, \quad (\text{Poisson equation}) \quad \omega = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$$

$$\partial_t \omega + u \cdot \nabla \omega = \nu \Delta \omega, \quad \text{Helmholtz equations.}$$

$$\text{If } \nu=0, \text{ (inviscid fluid) then: } \partial_t \omega + u \cdot \nabla \omega = \frac{\mathbf{d}\omega}{\mathbf{d}t} = 0,$$

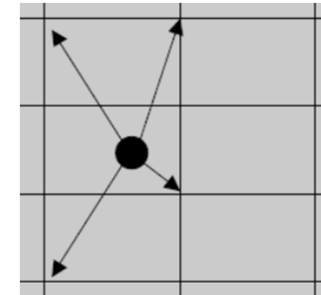
So in 2D the vorticity is constant along the trajectory

Computational algorithm in 2D:

1. Particle approximation and redistribution to the grid nodes :

$$\omega(\mathbf{x}) = \sum_{p=1}^N \alpha_p \delta(\mathbf{x} - \mathbf{x}_p); \quad \alpha_{p(i)} = \int_{V_p} \omega_i(\mathbf{x}) d\mathbf{x} \approx h^2 \omega_i(\mathbf{x}_p)$$

$$\omega_j = \sum_p \alpha_p \Lambda_j(\mathbf{x}_p)$$



2. Solution of the Poisson equation for stream function and calculation of the velocity

$$\Delta \psi = -\omega, \quad u = \frac{\partial \psi}{\partial y}, \quad v = -\frac{\partial \psi}{\partial x}$$

3. Displacements of the particles :

$$\frac{d\mathbf{x}}{dt} = \mathbf{u}$$

4. Simulation of viscosity and realisation of non-slip boundary condition

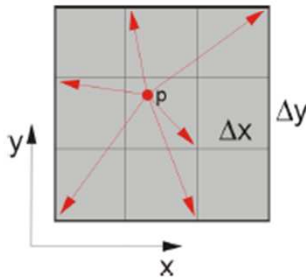
REDISTRIBUTION

INTERPOLATION FUNCTIONS

After particles movement, in order to solve the diffusion equation, it is necessary to transform the information about vorticity from the particles onto mesh nodes

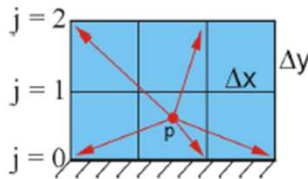
$$\omega_j = \frac{1}{h^2} \sum_p \Gamma_p \varphi\left(\frac{x - x_p}{h}\right)$$

- Particle inside of the domain



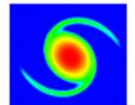
$$\varphi(x) = \begin{cases} 1 - \frac{5}{2}x^2 + \frac{3}{2}|x|^3 & |x| < 1 \\ \frac{1}{2}(2 - |x|)^2(1 - |x|) & 1 \leq |x| \leq 2 \\ 0 & |x| > 2 \end{cases}$$

- Particle near the wall



$$\varphi(x) = \begin{cases} 1 - \frac{1}{2}x^2 - \frac{3}{2}|x| & j = 0, |x| \leq 1 \\ -x^2 + 2|x| & j = 1, |x| \leq 1 \\ \frac{1}{2}x^2 - \frac{1}{2}|x| & j = 2, |x| \leq 1 \end{cases}$$

Both interpolation kernels conserve three first moments $I_\alpha = \sum_p x^\alpha \Gamma_p$, $\alpha = 1, 2, 3$



Simulation of viscosity

1. Stochastic approach (Chorin, JFM 1973):

The particle path is regarded as a stochastic process defined by Ito stochastic differential equation:

$$dX(\mathbf{x}_p, t) = \mathbf{u}(\mathbf{x}_p, t)dt + \sqrt{2\nu} dW(\mathbf{x}_p, t), \quad p = 1, \dots, N$$

$$\mathbf{x}_p^{n+1/2} = \mathbf{x}_p^n + \Delta t \mathbf{u}^n(\mathbf{x}_p)$$

$$\mathbf{x}_p^{n+1} = \mathbf{x}_p^{n+1/2} + \sqrt{2\nu\Delta t} \mathbf{N}_p$$

$$N^{(1)} = \cos(2\pi U^{(1)})\sqrt{-2\ln(U^{(2)})}$$

$$N^{(2)} = \sin(2\pi U^{(1)})\sqrt{-2\ln(U^{(2)})}$$

2. Simulation of the viscosity by Particle-Strength Exchange (PSE) method

$$\nu\Delta_h \omega|_p = \nu \frac{1}{h^2} \sum_{q=1}^N (\alpha_q - \alpha_p) \Lambda\left(\frac{\mathbf{x}_p - \mathbf{x}_q}{h}\right)$$

Realisation of the no-slip boundary condition

No-slip condition is realized by generation of the proper amount of the vorticity on the wall. The distribution of the vorticity inside of the flow domain generates non-zero tangent velocity at the wall u_s .

This undesirable tangent velocity can be canceled by proper vorticity flux:

$$\left. \frac{du}{dt} \right|_{Wall} \approx \frac{u(t + \Delta t) - u(t)}{\Delta t} = -\frac{\partial p}{\partial x} - \nu \frac{\partial \omega}{\partial y}$$

$$\frac{\partial \omega}{\partial t} = \nu \Delta \omega,$$

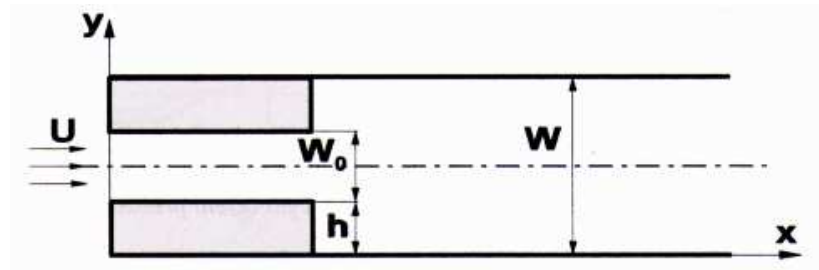
$$\omega(x, y, 0) = 0,$$

$$\frac{\partial \omega}{\partial n} = -\frac{\gamma}{\delta t \cdot \nu}.$$

$$\frac{\partial \omega}{\partial y} = -\frac{u_s}{\nu \Delta t}$$

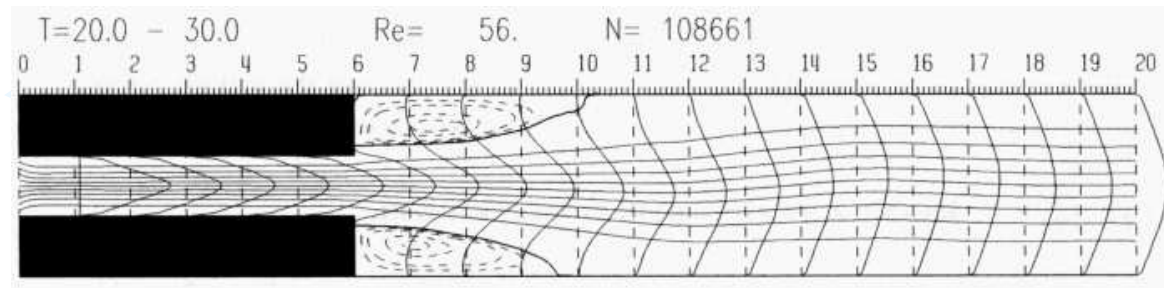
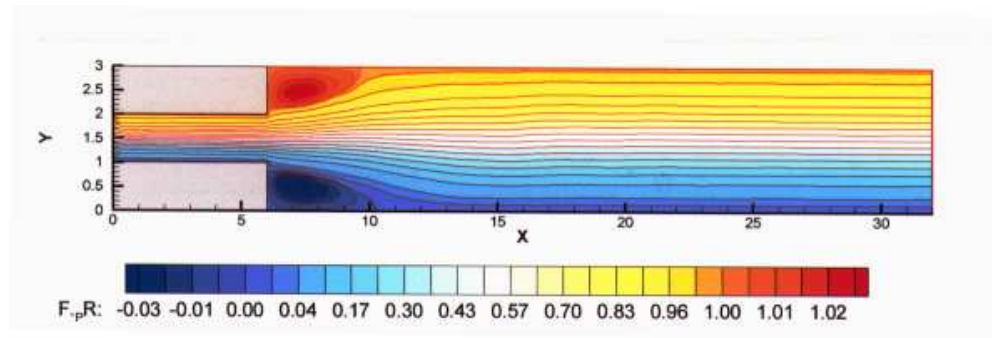
$$\omega_{new} = \omega_{old} + \omega_{gen}$$

Flow in channel with symmetric sudden expansion

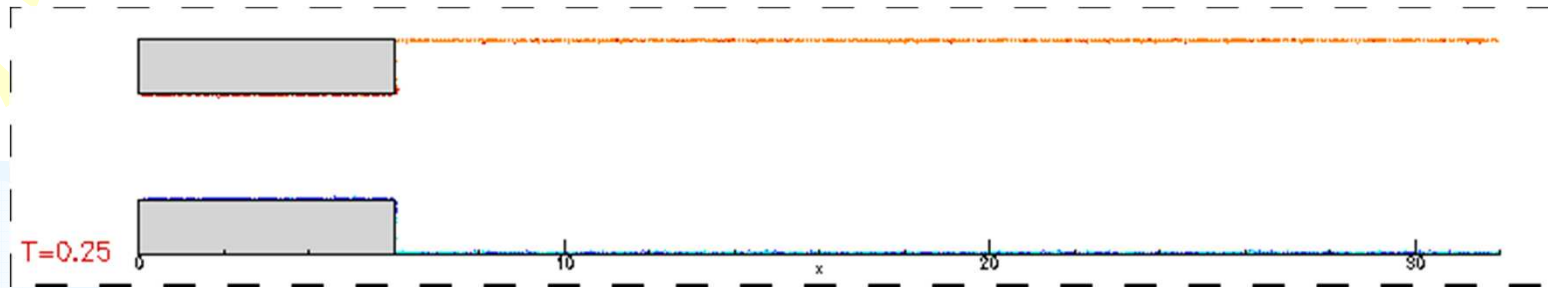


$$Re = \frac{Uh}{\nu}$$

$Re=56$



Flow in channel with symmetric sudden expansion cont.

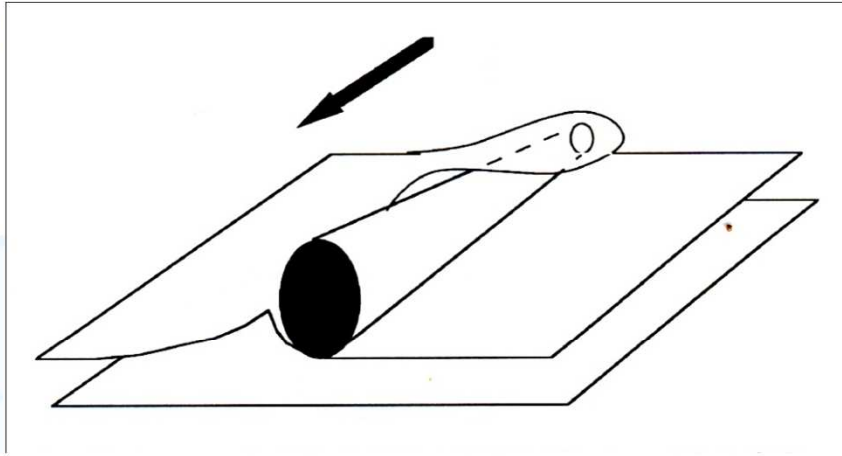


H.Kudela, Task Quart,3 1999

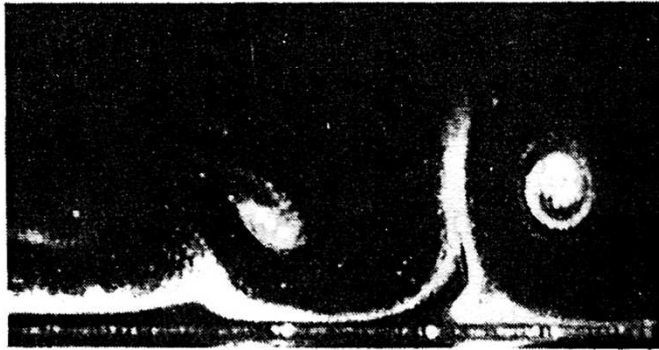


(Experiment by Durst, Melling, Whitelaw, JFM 1974)

Eruption of the Boundary Layer- Motivation



surface eruption



streamwise
vortex

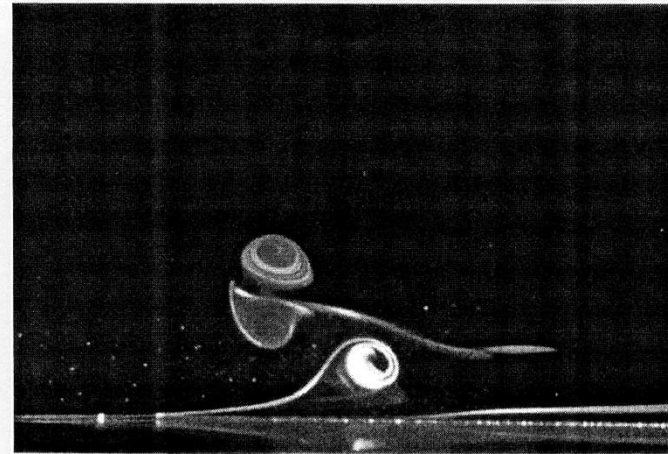
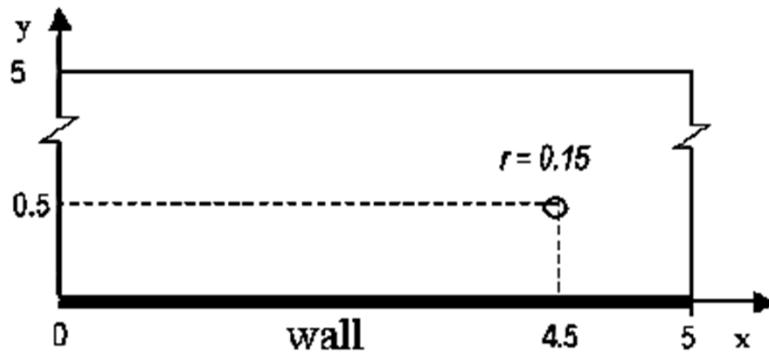


Fig. 20. Experiment demonstrating secondary vortex birth.
Photo courtesy of M. Stanislas and P. DuPont, Ecole Centrale
de Lille. [Panton, 2001, JPAS](#)

[Doligalski, Smith, Walker, 1994, Ann. Rev. Fluid Mech.](#)

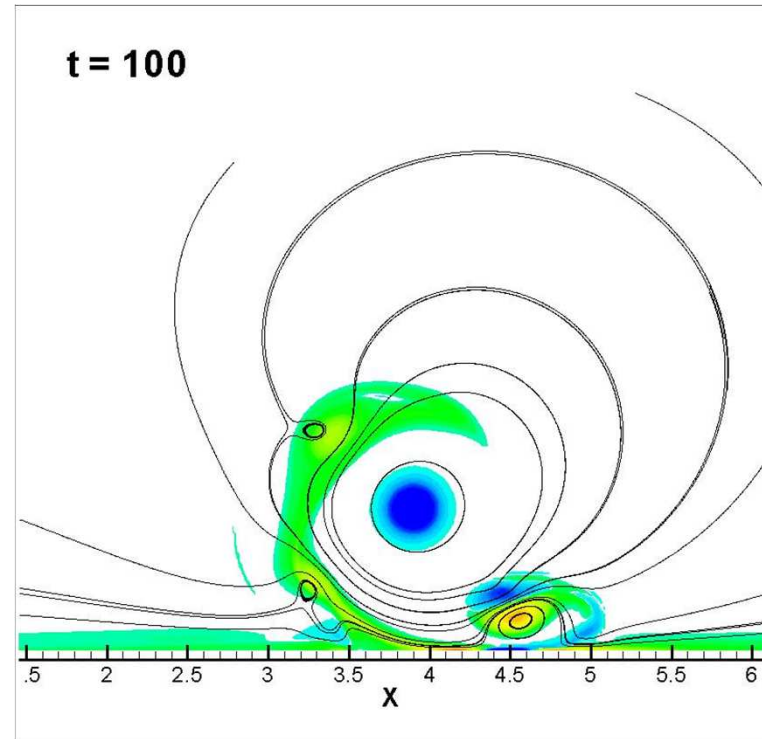
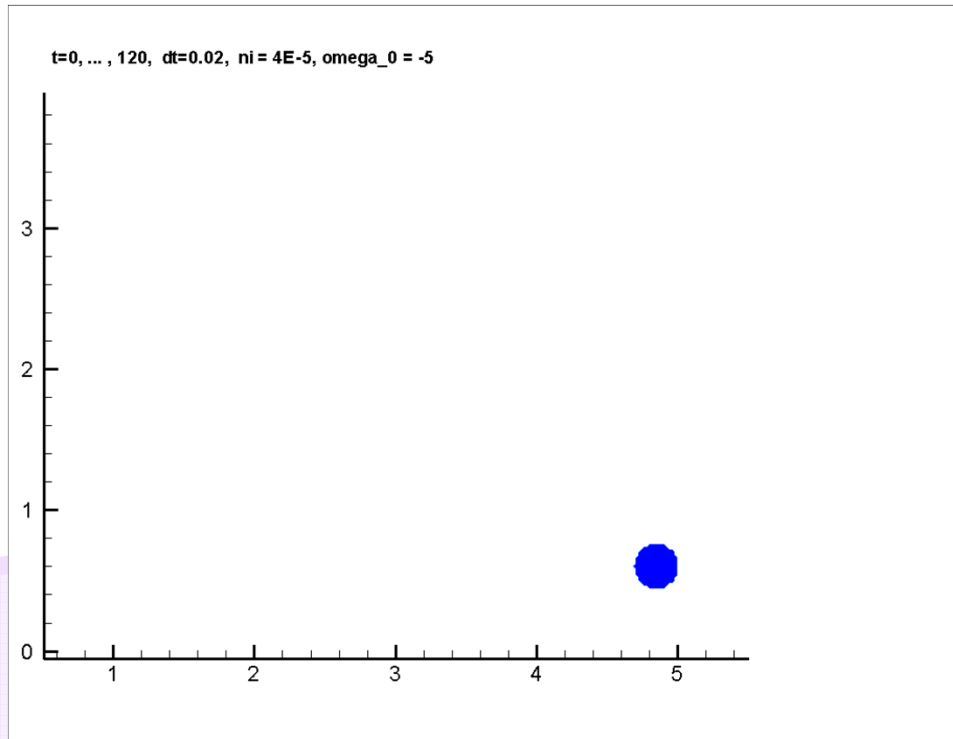
Problem formulation



$$\omega_t + \mathbf{u} \cdot \nabla \omega = \nu \Delta \omega$$

$$\Delta \psi = -\omega, \quad u = \partial_y \psi, \quad v = -\partial_x \psi \quad (1)$$

$$\psi|_{x=0} = \psi|_{x=L}, \quad \psi|_{y=0} = \psi|_{y=top} = 0$$

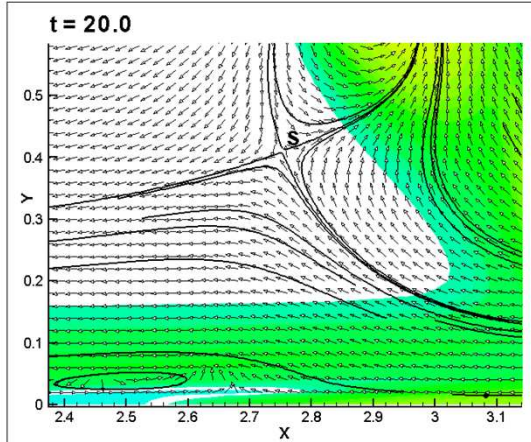
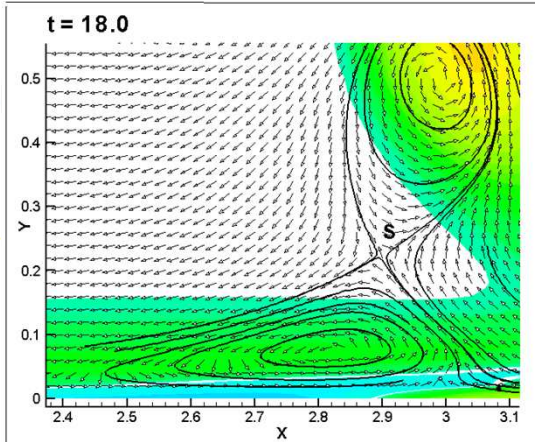
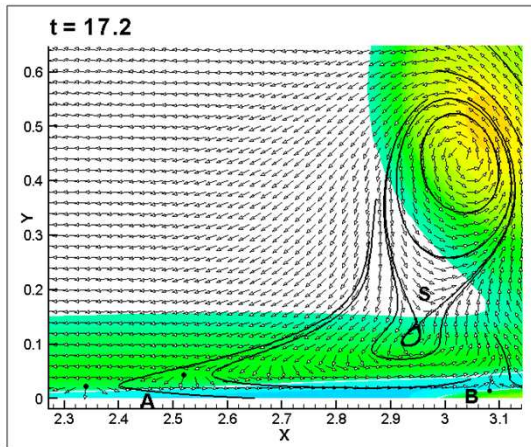
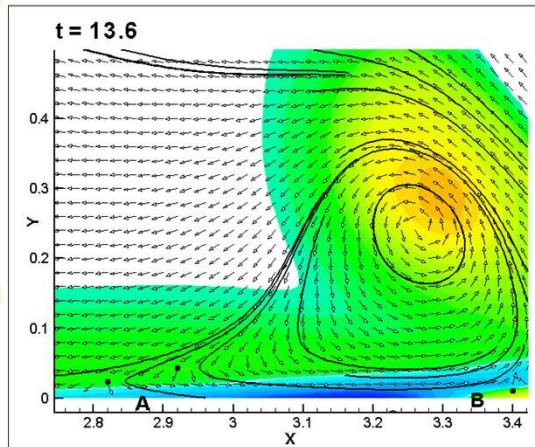


H.Kudela, Z. Malecha
Fluid Dyn. Res., 41,2009

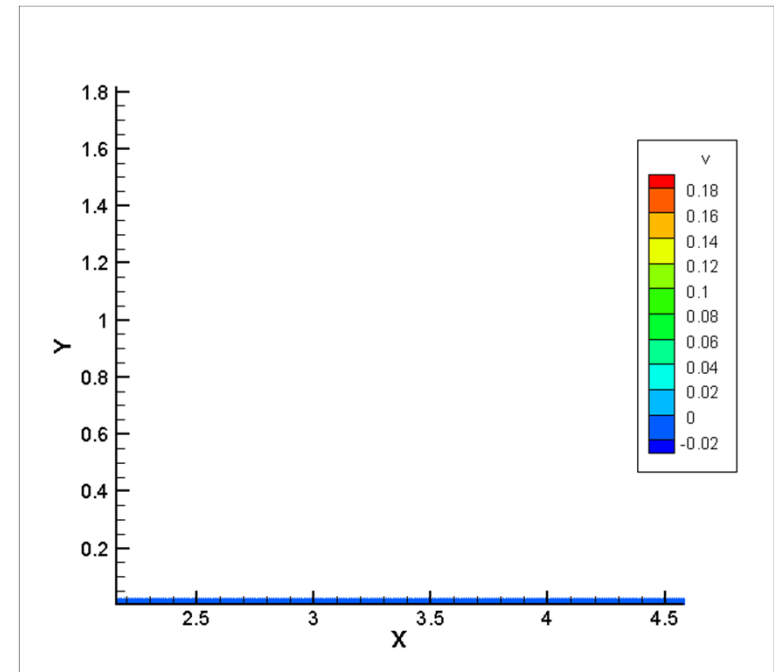
$Re = 17670; \nu = 0.0002$

$Re = \Gamma/\nu$

The sequence of induced secondary vortex structures

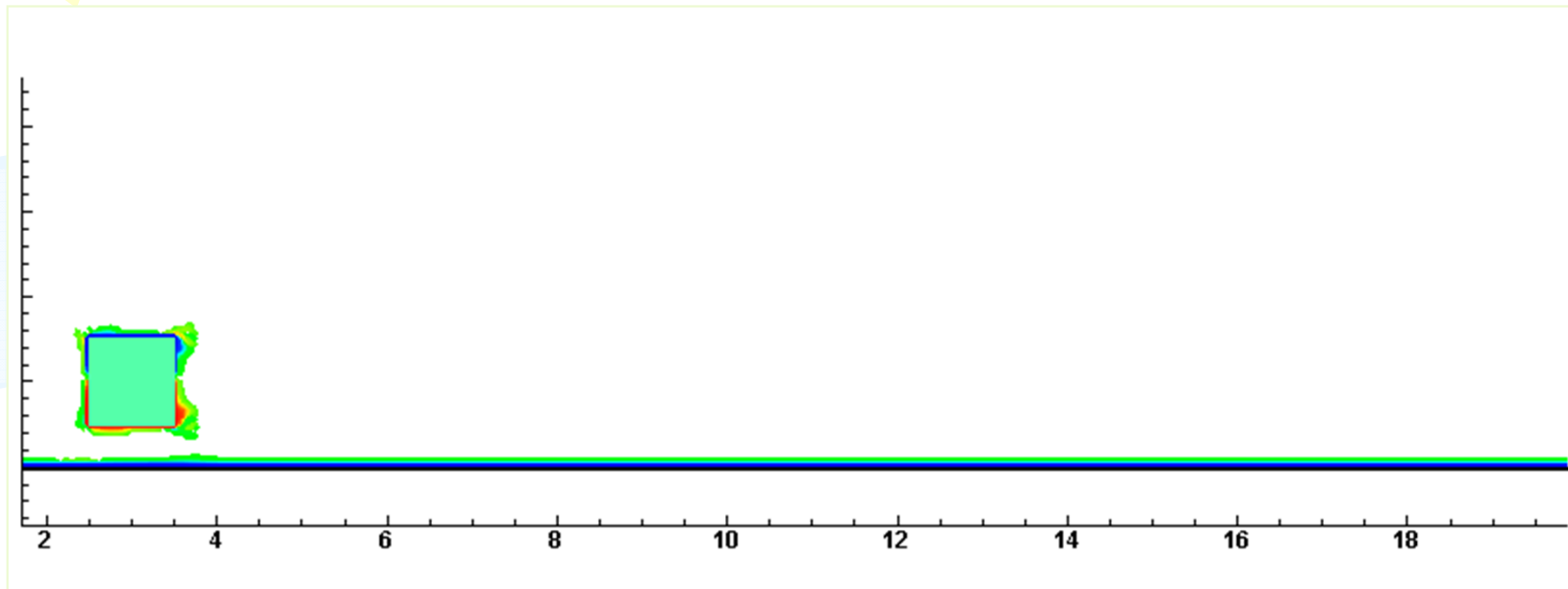


Animation of passive markers from the boundary region



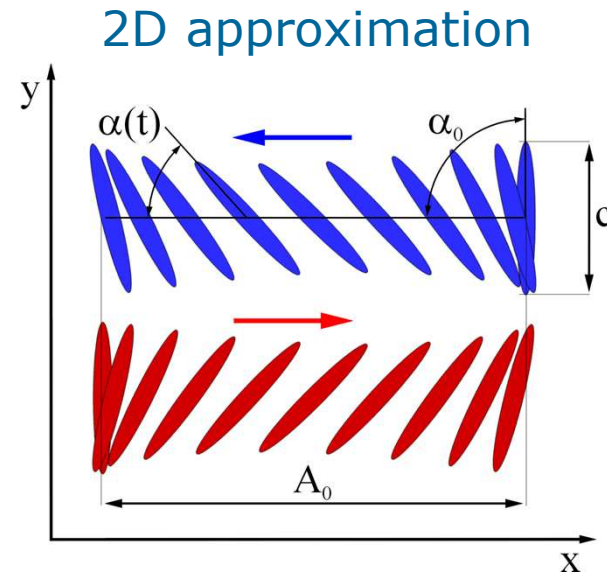
Streamlines with the velocity directions and vorticity in the fond.

Interaction of the Vortex with the Wall

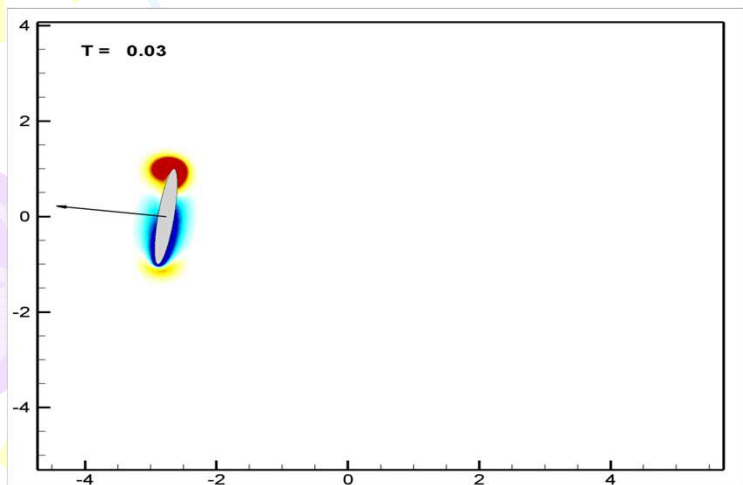


Z. Malecha, *PhD. Thesis, 2009*

Flying insects



Re=75 vorticity field



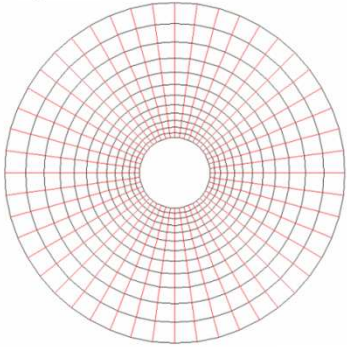
Center of the wing movement

$$\alpha(t) = \alpha_0 + \alpha_A \cos(2\pi ft)$$

$$[x(t), y(t)] = A_0 \cos(2\pi ft) [\cos(\beta), \sin(\beta)]$$

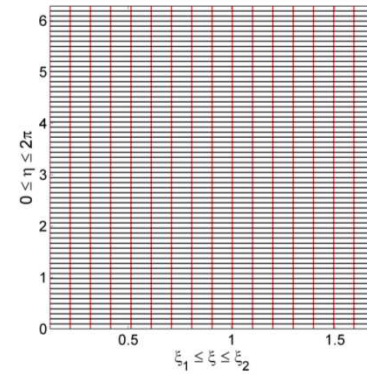
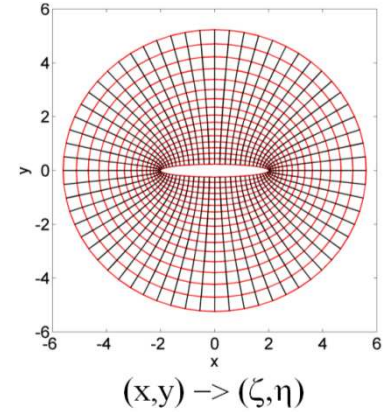
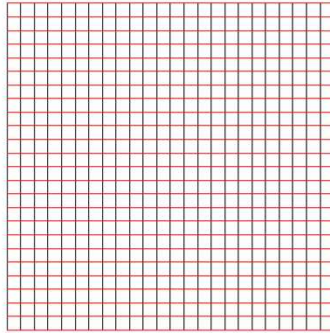
Conformal Mapping

a)

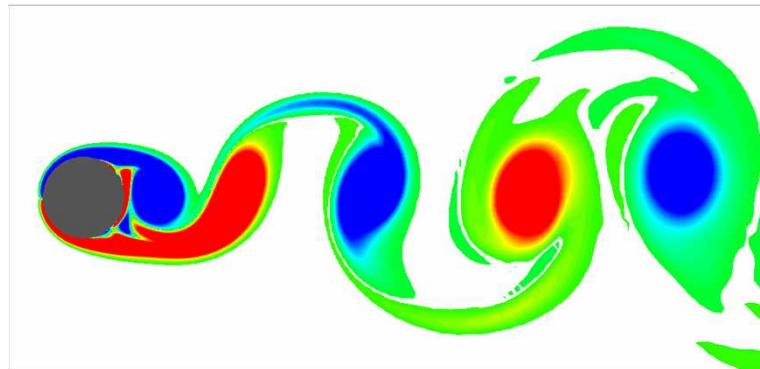


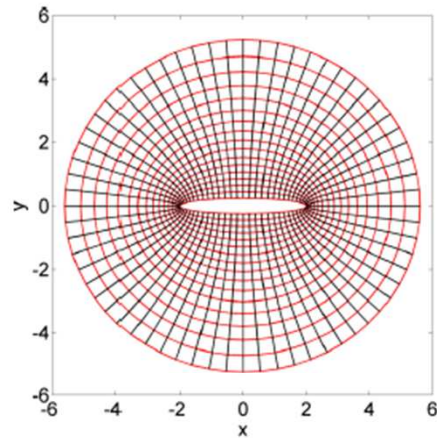
$(x,y) \Rightarrow (\zeta,\eta)$

b)

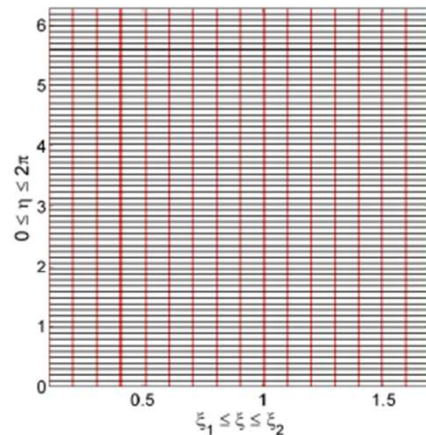


$$x + iy = \exp(r + i\theta)$$





$(x,y) \rightarrow (\xi,\eta)$



In new variables (ξ, η) the equations of motion are

$$\frac{\partial \omega}{\partial t} + u \frac{\partial \omega}{\partial \xi} + v \frac{\partial \omega}{\partial \eta} = \frac{\nu}{J} \Delta \omega$$

$$\Delta \psi = -J \omega$$

where J denotes Jacobian of the conformal transformation

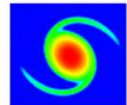
$$J = \det \begin{vmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial x}{\partial \eta} \\ \frac{\partial y}{\partial \xi} & \frac{\partial y}{\partial \eta} \end{vmatrix}$$

The velocity field is determined with the formulas

$$u = \frac{1}{J} \frac{\partial \psi}{\partial \eta}, \quad v = -\frac{1}{J} \frac{\partial \psi}{\partial \xi}$$

THE MAIN ADVANTAGE OF CONFORMAL MAPPING APPLICATION:

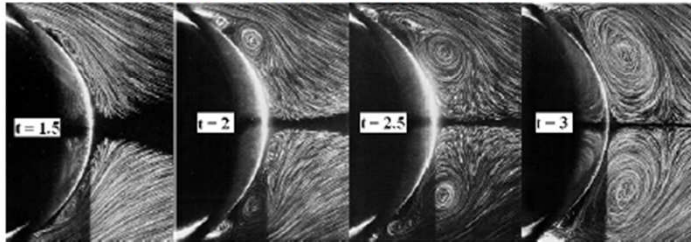
by the conformal mapping the physical non-rectangular flow region (x, y) is replaced by the rectangular one (ξ, η) , in which the fast Poisson solvers can be used.



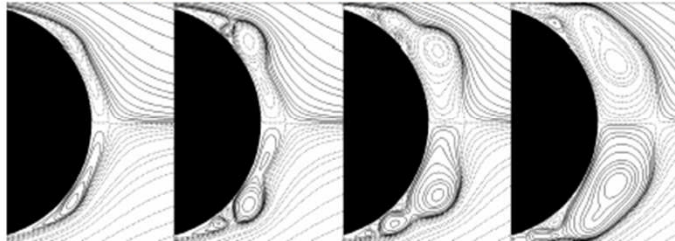
TEST OF THE VIC METHOD

- FLOW OVER CYLINDER

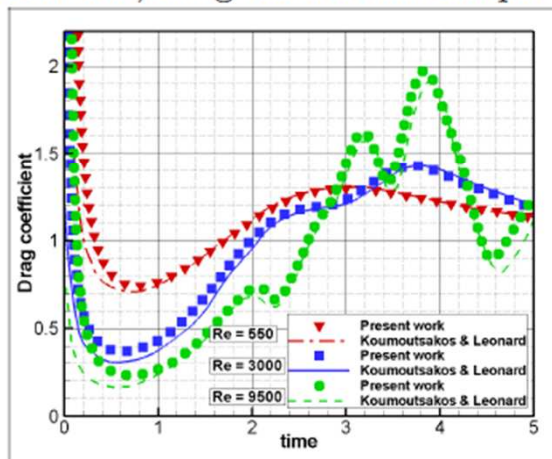
experiment, $Re = 9500$



calculation, stream function



calculation, drag coefficient comparison

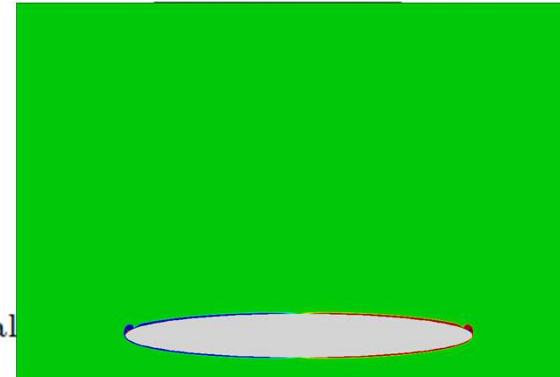


- FLOW OVER ELLIPSE, $Re = 10000$

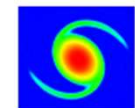
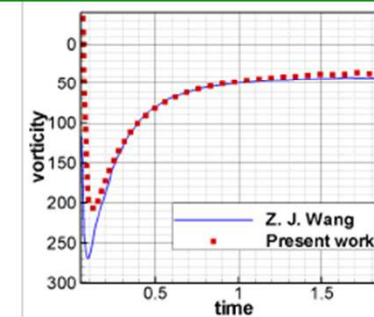
experiment



calculation, vorticity field



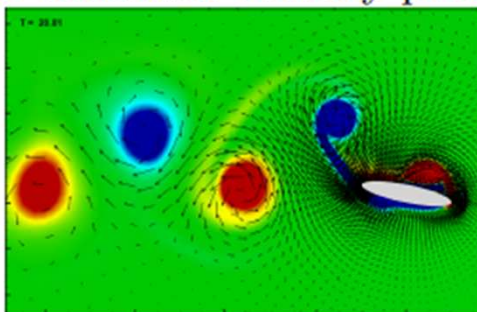
calculation, drag coefficient comparison



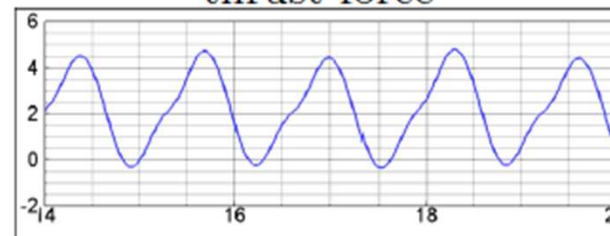
The change of topology of vortex street



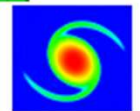
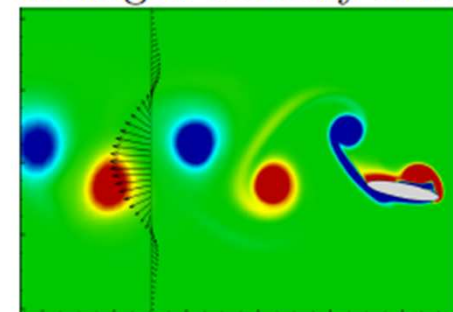
the transient velocity profile



thrust force



averaged velocity field

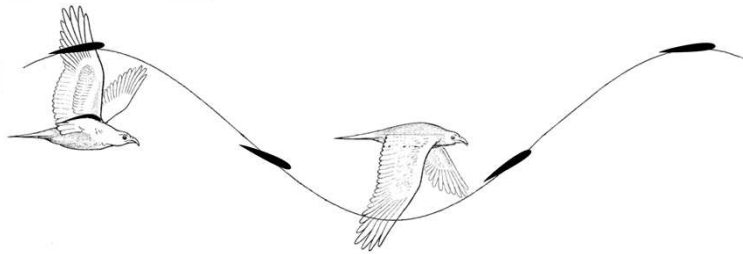


Flapping scheme in living nature

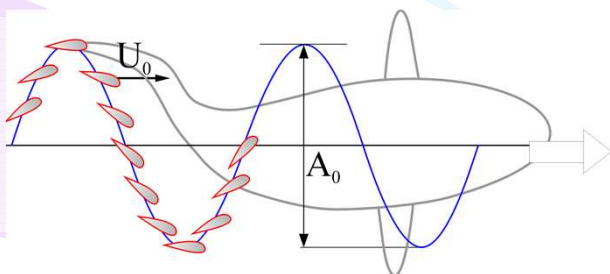
Insects



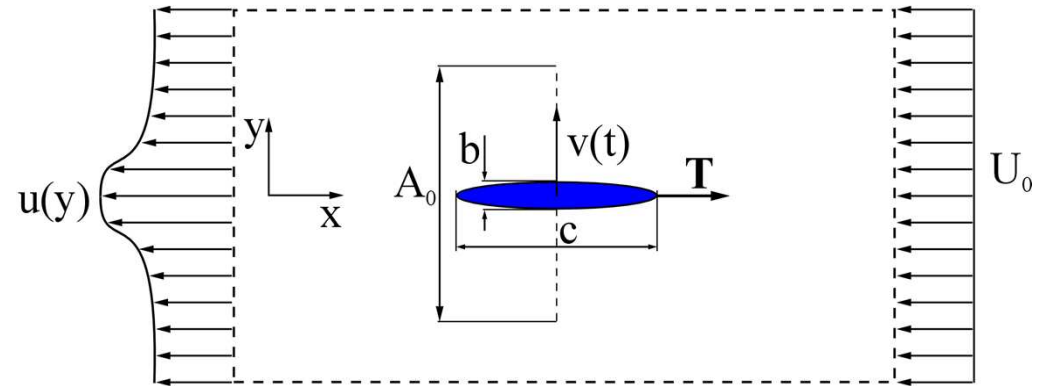
Birds



Fishes



Simplification



Foil oscillation

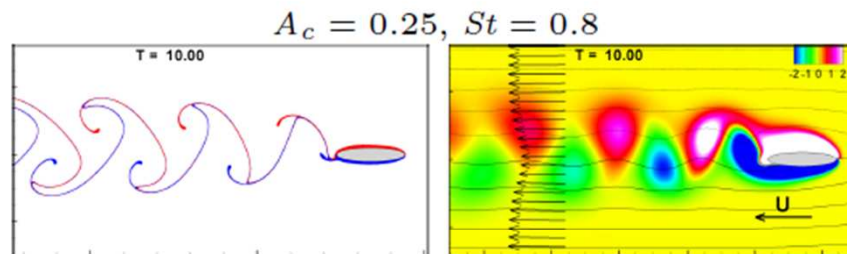
$$y(t) = \frac{A_0}{2} \sin(2\pi ft)$$

Flapping system can be analysed in terms of three main non-dimensional parameters

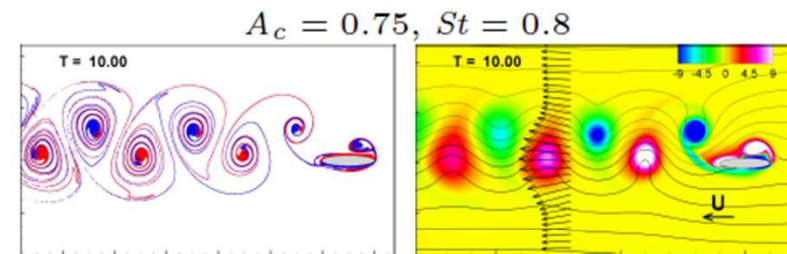
$$Re = \frac{U_0 c}{\nu}, \quad St = \frac{fc}{U_0}, \quad A_c = \frac{A_0}{c}$$

Transitions of the vortex street of a flapping foil, $Re = 100$

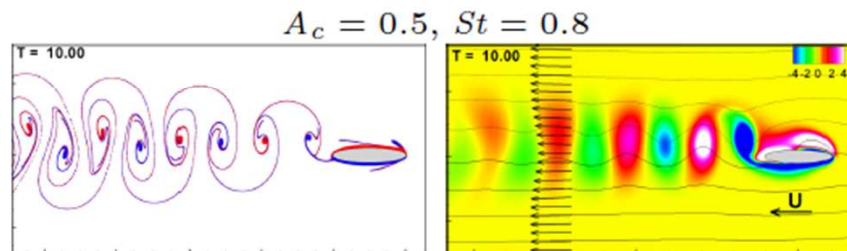
1 Karman vortex street



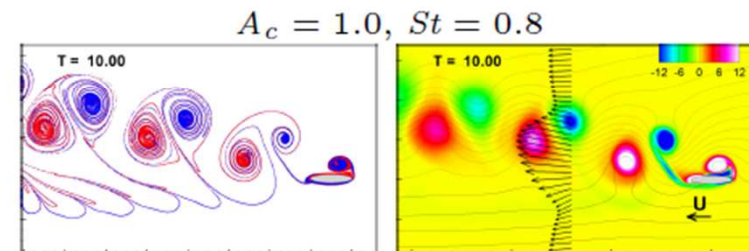
3 reversed Karman vortex street



2 aligned vortices

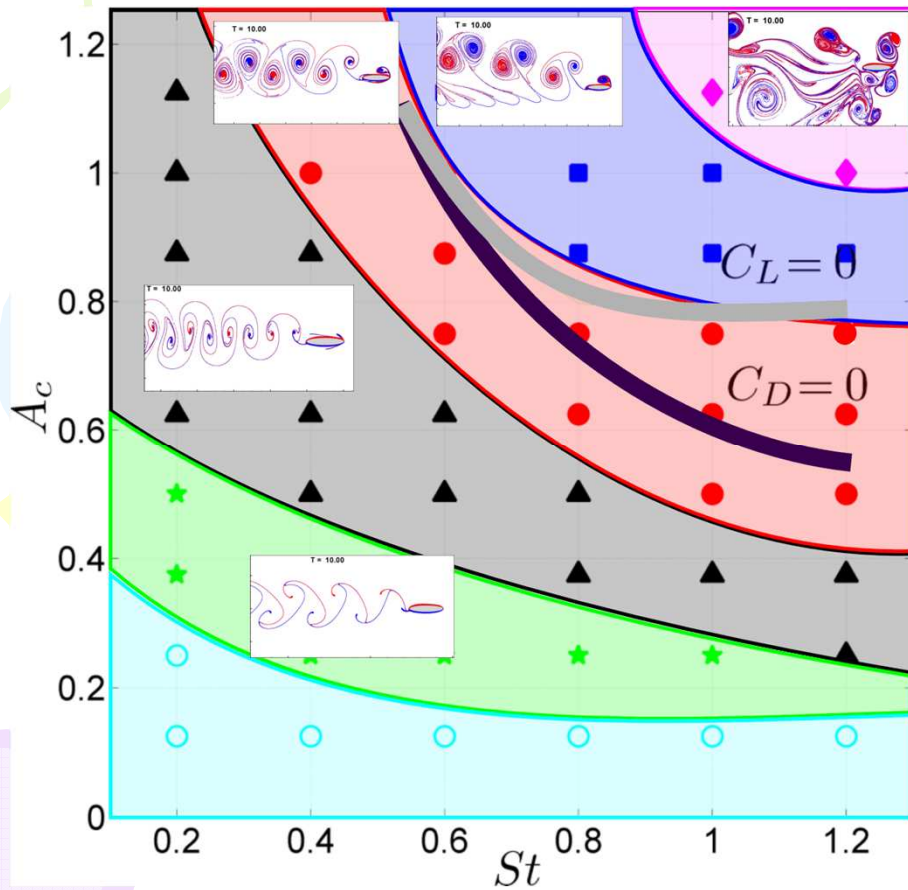


4 deflected reversed Karman vortex street



$$St = \frac{fc}{U_0}, \quad A_c = \frac{A_0}{c}$$

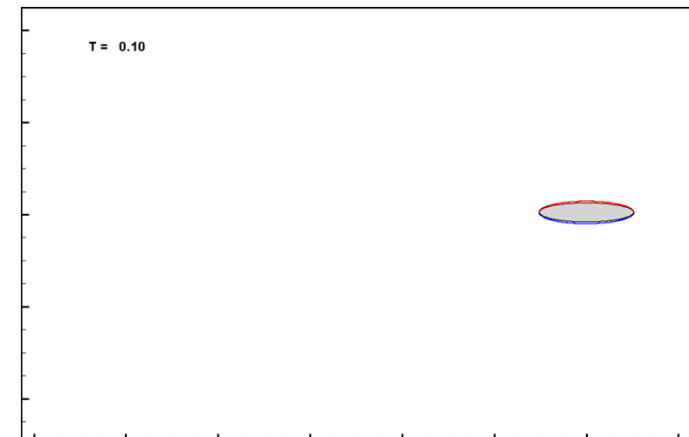
Phase transition diagram



Deflected vortex wake,
thrust and lift force



Chaotic vortex wake

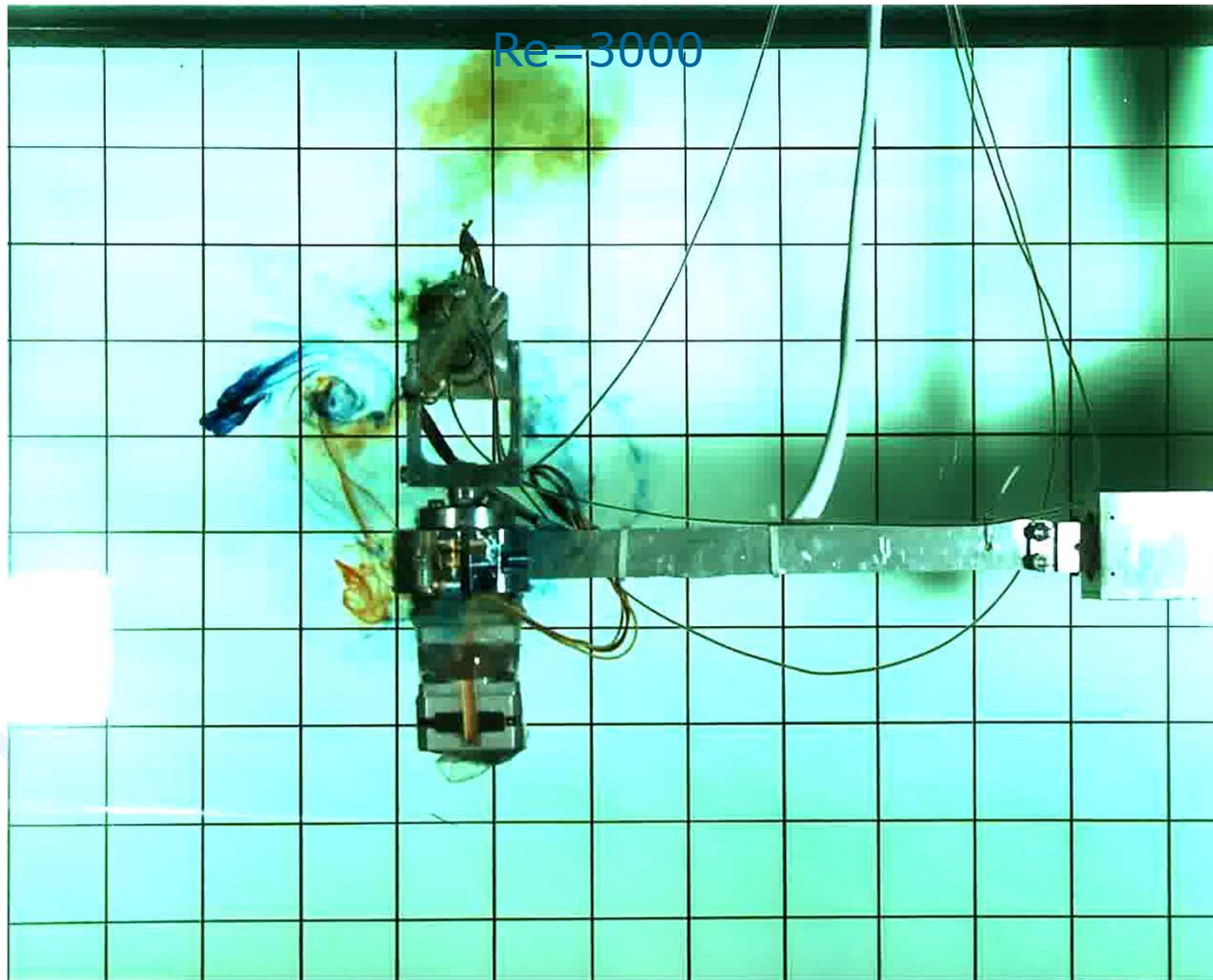


Department of Aerospace Engineering
prof. K. Sibilski group



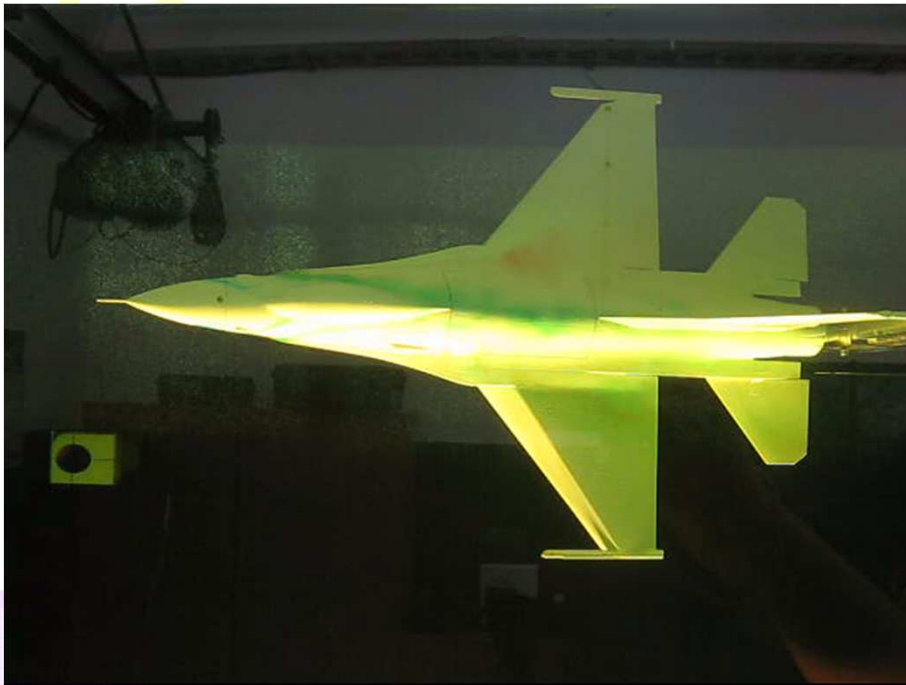
The Rolling Hills Research Corporation Flow Visualization Water Tunnel

Flapping mechanism

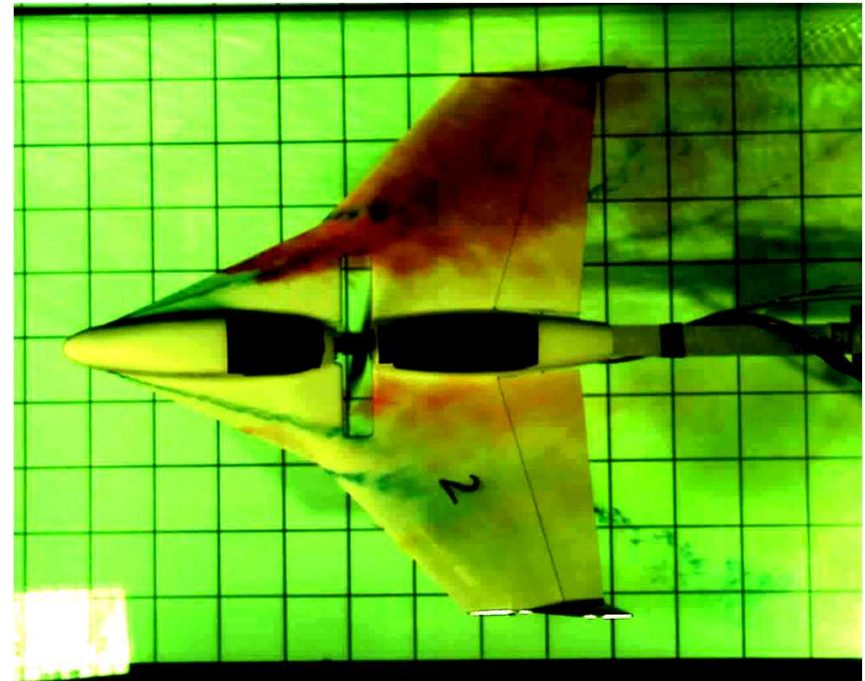


P. Czkałowski, Department of Aerospace Engineering

Flow Visualizations



F-16



UAV project

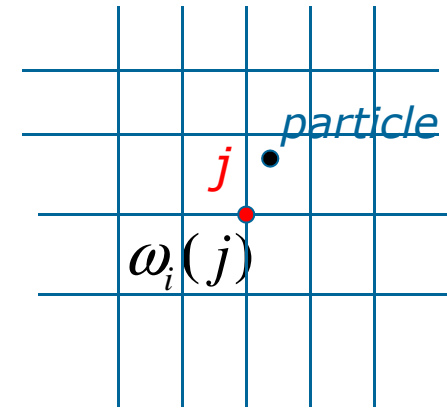
Department of Aerospace Engineering, prof. K. Sibilski, dr Gronczewski

3D VORTEX IN-CELL

The velocity of the particles are calculated by solving Poisson equations by finite difference method for vector potential:

$$\Delta A_i = -\omega_i, \quad i = 1, 2, 3$$

To obtain the grid values for $\omega_i(j)$ the redistribution of weights particles process must by done:



$$\omega_{i,j} = \begin{cases} \frac{\sum_p \alpha_p \varphi_j(\mathbf{x}_p)}{J_j}, & J_j \neq 0 \\ 0, & J_j = 0 \end{cases}$$

$$J_j = \sum_p h^3 \varphi_j(\mathbf{x}_p) \approx h^3$$

φ_j – 3D B-spline of 3th order

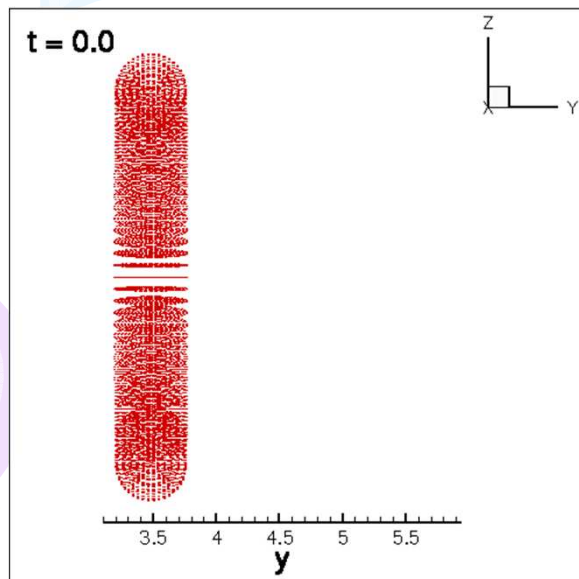
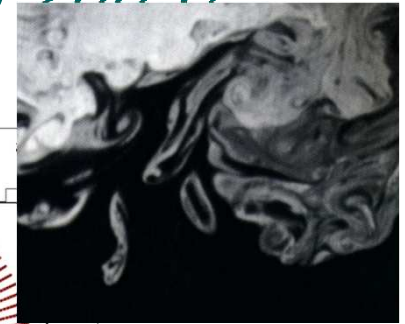
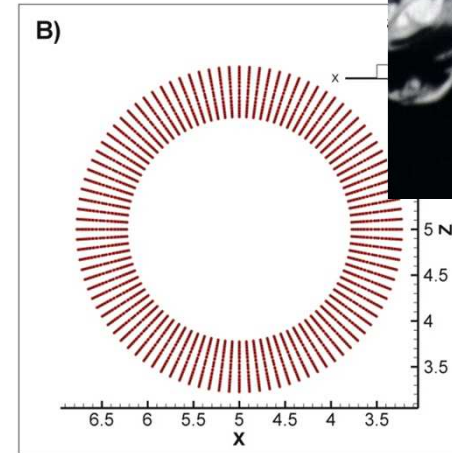
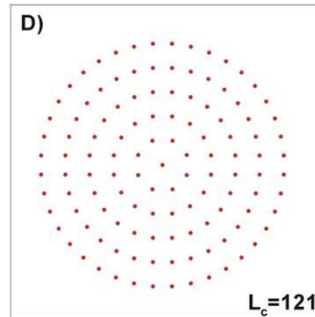
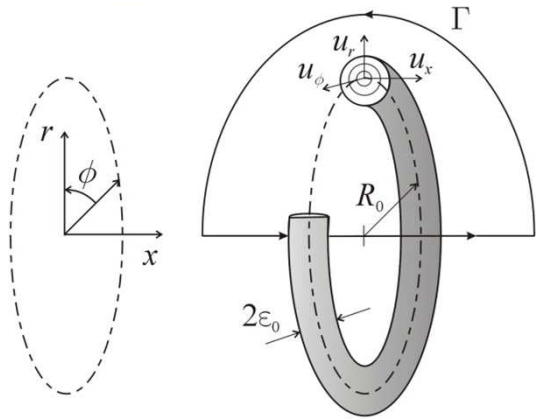
Velocity on the grid nodes is calculated by finite differences

$$\mathbf{u}(\mathbf{x}_j) = \nabla \times \mathbf{A}$$

Velocity of the particles is obtained by the interpolation:

$$\mathbf{u}(\mathbf{x}_p) = \sum_j \mathbf{u}(\mathbf{x}_j) L_j(\mathbf{x}_p)$$

VORTEX RING MOTION (Regucki, Ph.D 2003)



Geometrical parameters of the ring:

- inner radius $r_0 = 0.3$
- outer radius $R_0 = 1.5$
- circulation $\Gamma = 1.0$

- number of the grid nodes: $i = j = k = 101$
- $\Delta x = \Delta y = \Delta z = h = 0.1$
- time step: $\Delta t = 0.02$
- number of vorticity-particles: $N = 12100$

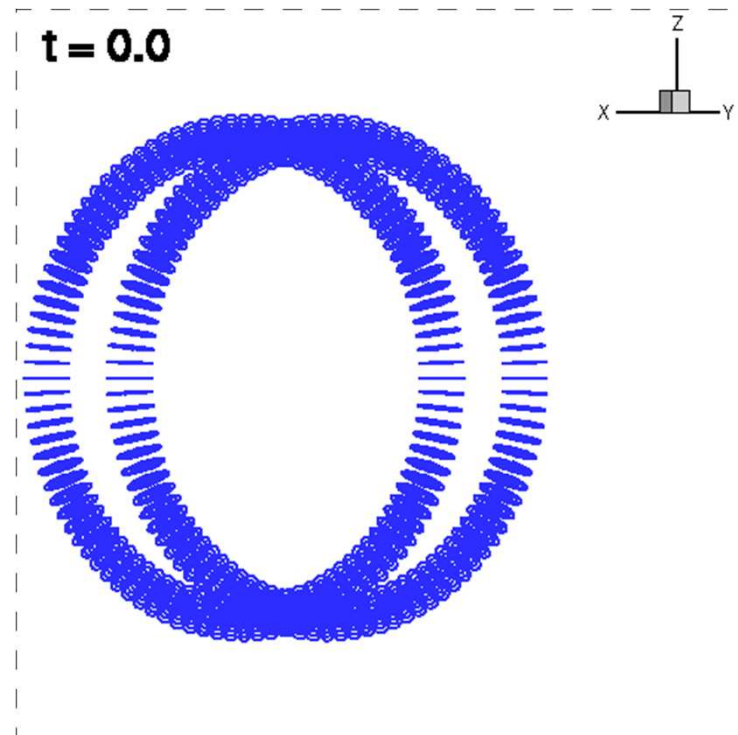
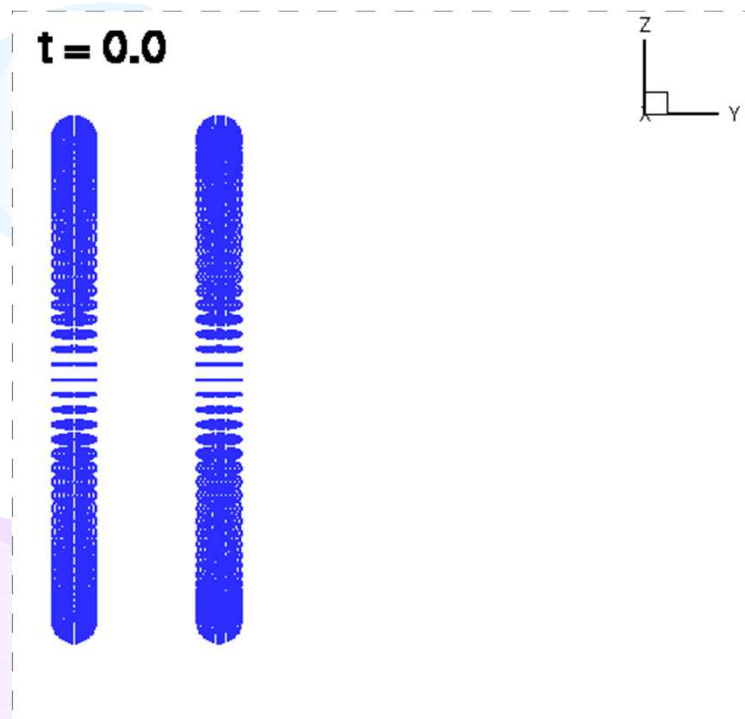
VORTEX GAME (Leap-frogging)

Kudela, Regucki, ICCS, 2004

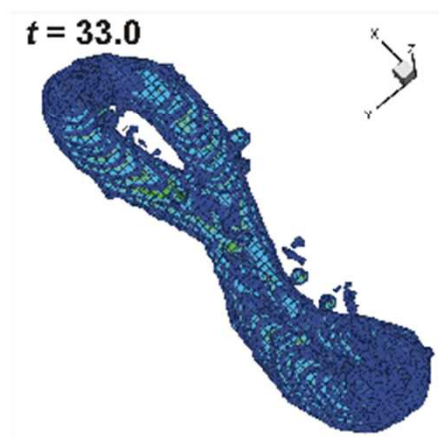
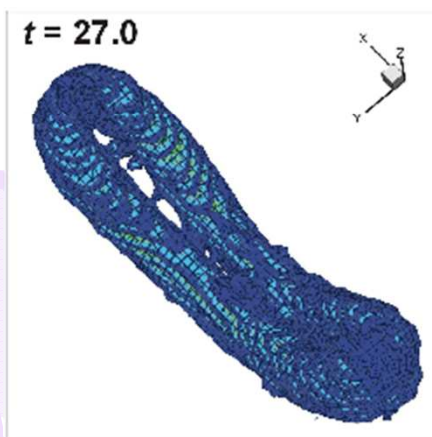
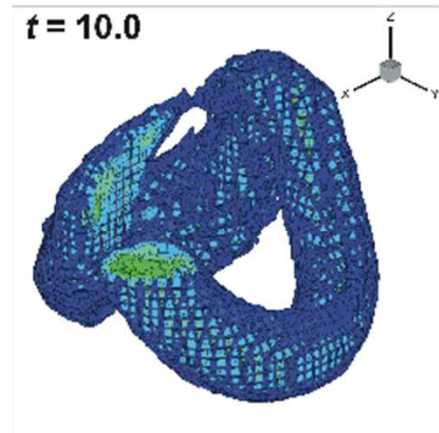
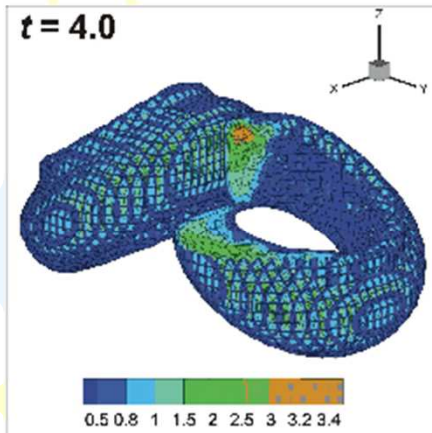
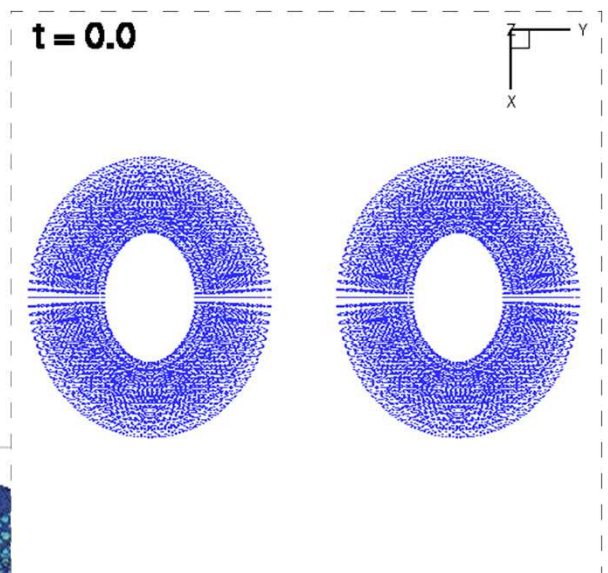
Parameters:

- $r_1 = 0.15, r_2 = 0.15$
- $R_1 = 1.5, R_2 = 1.5$
- $\Gamma_1 = 1.0, \Gamma_2 = 1.0$

- kinetic energy: $T_0 = 5.25$ -variation $\sim -3\%$,
- helicity $H_0 = 10^{-5}$,
- divergence of A, u, ω ; $\sim 10^{-5}$,

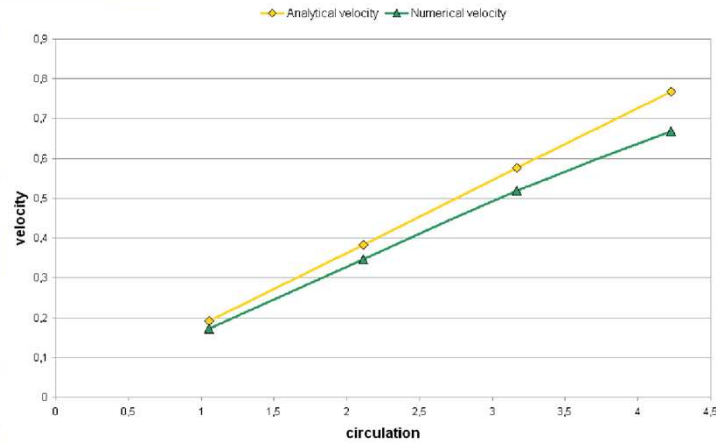


Reconnection of vortex rings

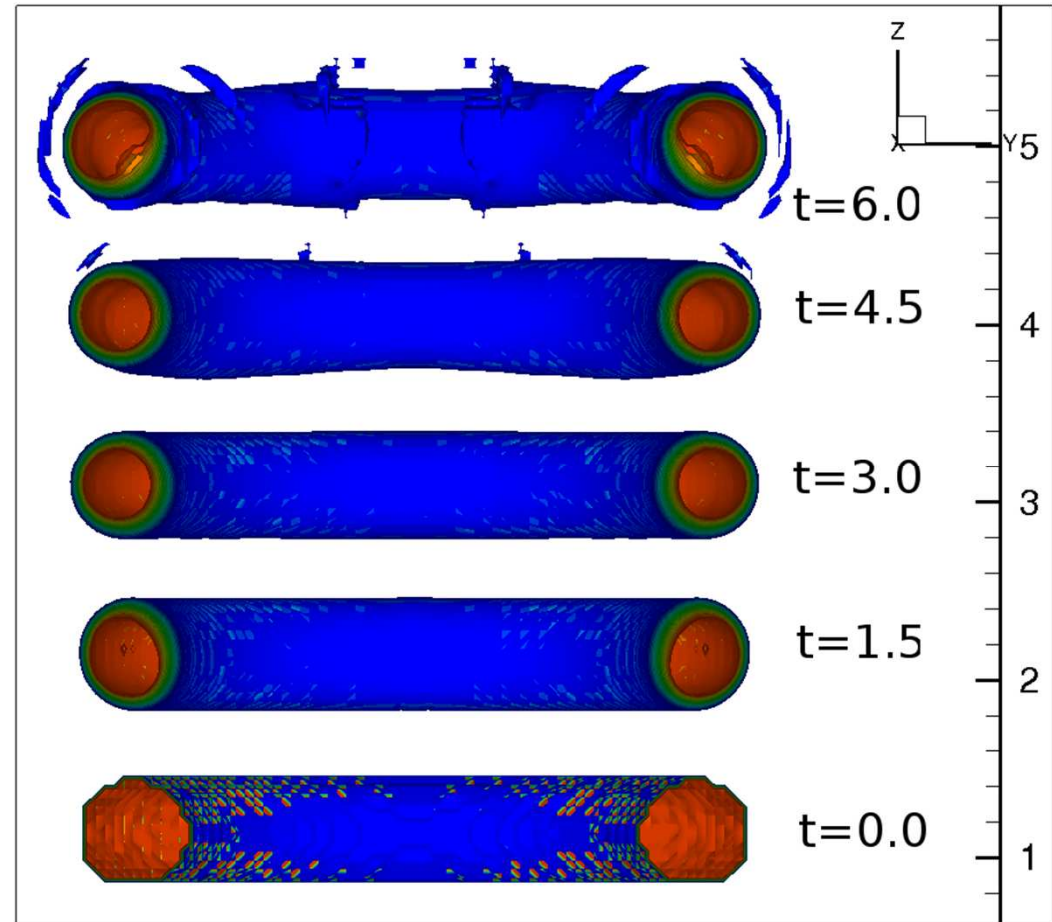
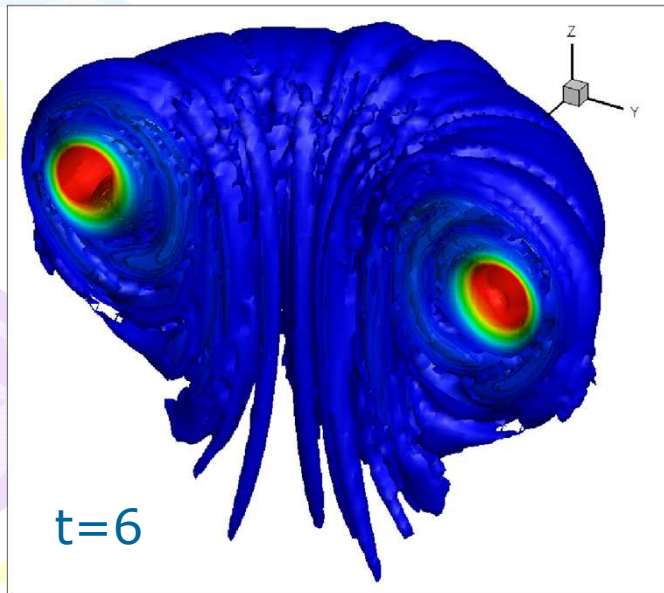


Parallel Computations – vortex ring

Andrzej Kosior, PhD. student



Analytical and numerical velocities of the vortex ring



Evolution of the vortex ring

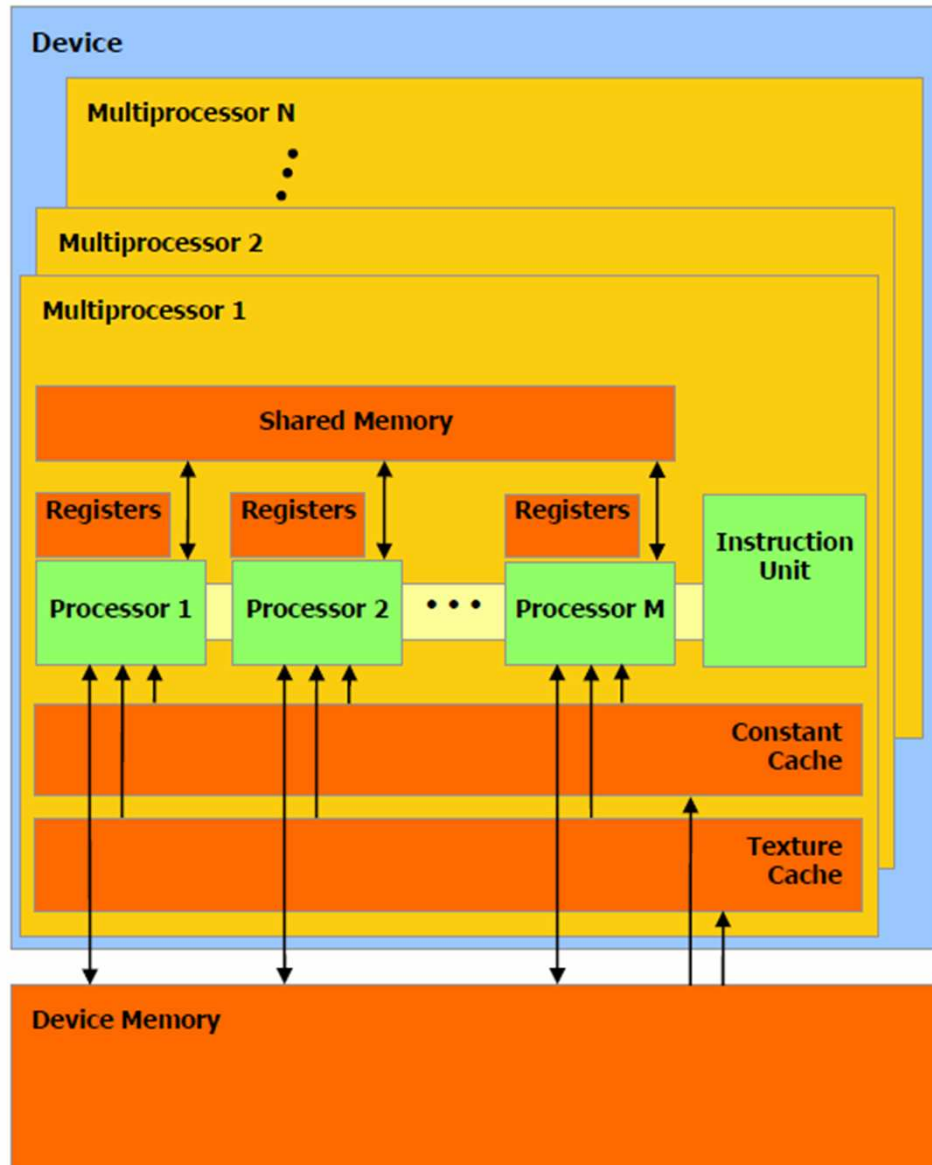
CUDA Hardware

CUDA hardware structure:

- multiprocessors,
- streaming processors,
- one instruction unit per multiprocessor,

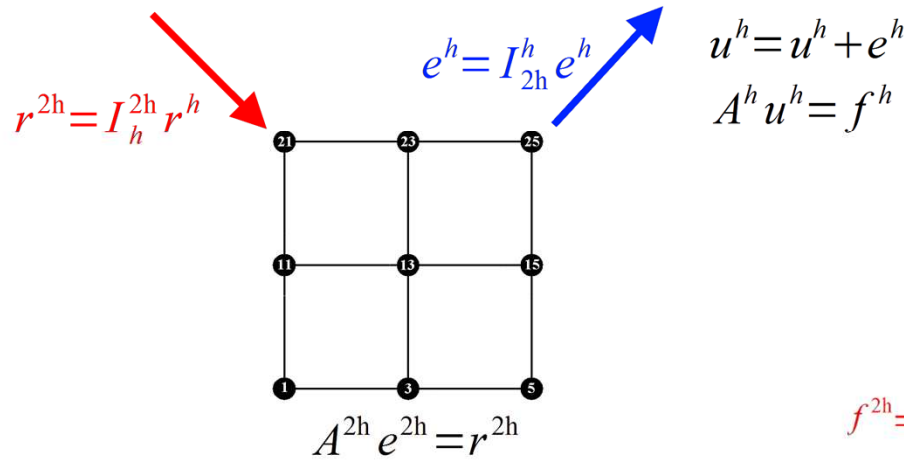
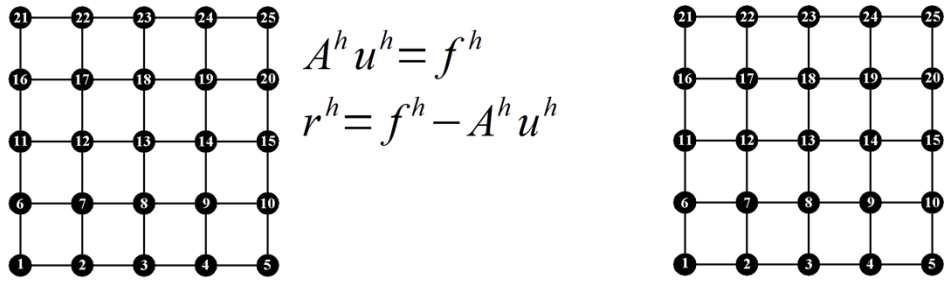
In CUDA architecture we can distinguish following memory types:

- device memory,
- texture memory,
- shared memory.

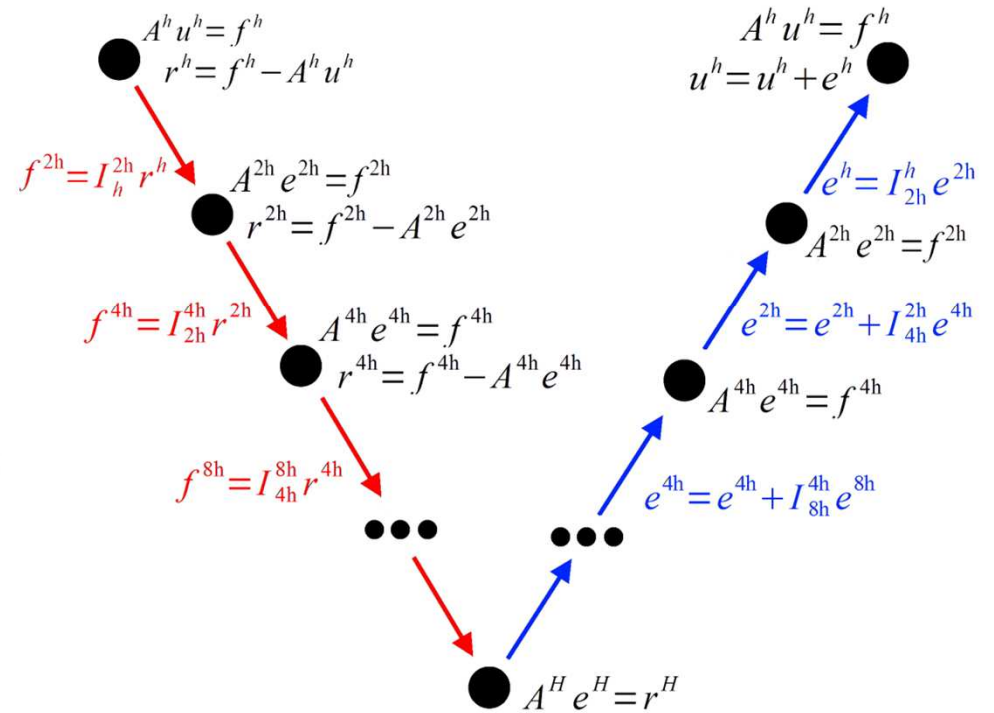


Multigrid method For Poisson equation

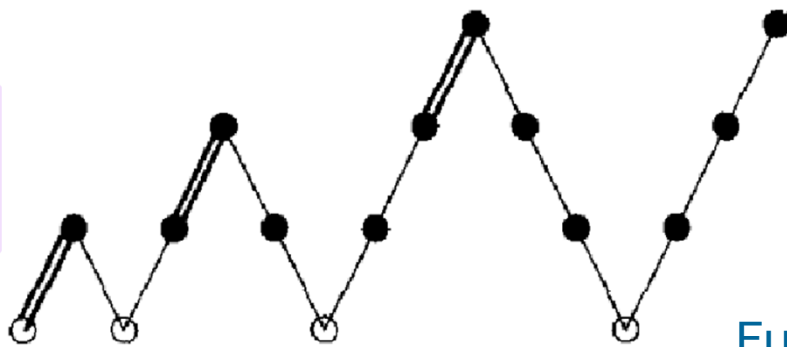
Multigrid method



Two-grid method



Full Multigrid Method

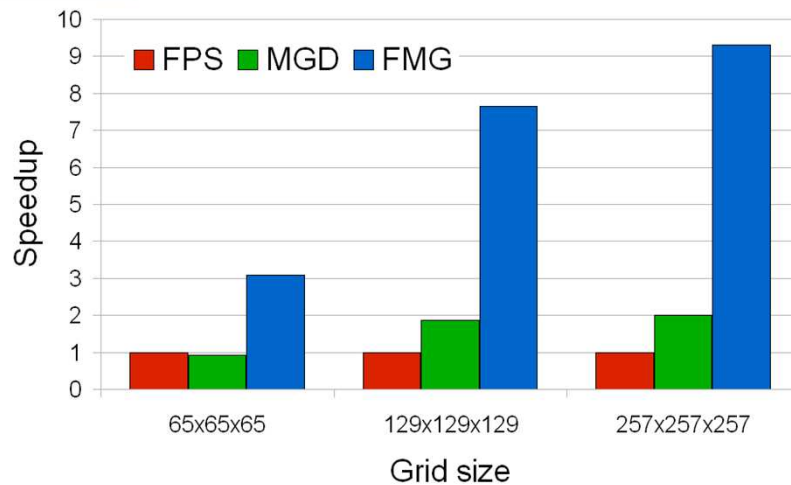


Test of Multigrid Method

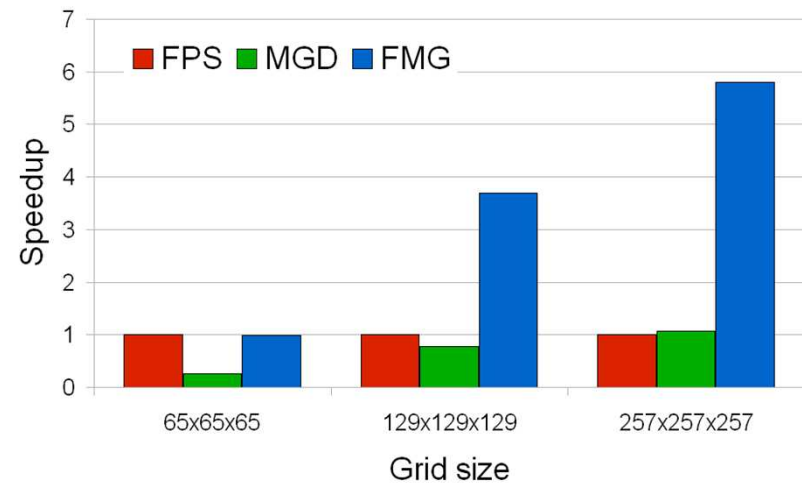
The test problem was a three-dimensional Poisson equation which solution was following function:

$$\psi(x, y, z) = \sin(2\pi x) \cdot \sin(2\pi y) \cdot \sin(2\pi z); x, y, z \in [0, 1]$$

There were two different boundary conditions tested.



Speed-up for Dirichlet boundary condition



Speed-up for periodical boundary condition

Computations were performed on:
CPU (Intel i7 960),
GPU (NVIDIA GeForce GTX 480).



Summary

- **Vortex Methods** provide natural, useful tools for analyzing the flow in terms of vorticity dynamics
- **VM** are robust and give reasonable results at a wide range of Reynolds number
- **3D VM** are very promising for parallel computations